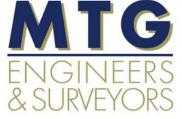
AEP AMERICAN SOUTHWESTERN ELECTRIC ELECTRIC POWER POWER COMPANY

WELSH POWER PLANT ASH LANDFILL

Run-on and Run-off Control System Plan Update & Reissue

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MTG TEXAS FIRM REGISTRATION NUMBER: <u>354</u> MTG PROJECT NUMBER: 217001

WELSH POWER PLANT - ASH LANDFILL Run-on and Run-off Control System Plan

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1.0 Introduction

The Welsh Power Plant has a deed recorded ash landfill (Phase 1 Landfill) that currently receives ash materials from two 528 MW coal fired boilers. The plant annually produces fly ash, bottom ash and economizer ash. Typically, bottom and economizer ash are sluiced to the Primary Ash Pond, which has been periodically dredged and temporarily stored in the Bottom Ash Storage Pond.

Welsh Units 1 and 3 were retrofitted in 2016 to capture mercury in order to comply with EPA Mercury and Air Toxics Standard (MATS) emissions regulations. Activated Carbon Injection (ACI) captures the mercury and is mixed with fly ash to form an ACI byproduct, which is captured in a Pulse Jet Fabric Filter (PJFF).

The Ash Landfill has traditionally been operated in two sections, with a portion of the landfill being primarily composed of dredged bottom ash, economizer ash, and fly ash material sluiced to the ash landfill between approximately 1986 and 2000. The western portion of the Ash Landfill is used to reclaim ash materials for beneficial reuse. Ash sales to the construction industry have helped to extend the Ash Landfill life. A contract ash marketer utilizes the western two-thirds of the Ash Landfill as a temporary storage and processing area for fly ash. The ash marketer is contracted to sell all marketable ash material for beneficial reuse in order to extend the life of the Ash Landfill.

Modifications to the Ash Landfill cap, cover and dewatering systems were incorporated into a landfill site development plan and implemented in 2016 through 2019 (two separate contract efforts). These modifications were submitted to the Texas Commission on Environmental Quality (TCEQ) Industrial Solid Waste Permits Section and each were acknowledged by same. The modifications included provisions for a minimum 3-foot thickness compacted clay cap and a minimum 1.5-foot thickness erosion/vegetative cover, in accordance with TCEQ Technical Guideline No. 3. A project was also conducted in 2017, adding the Low Water Crossing.

30 TAC 352.811 (and by reference 40 CFR 257.81) requires the owner or operator of an existing or new landfill or any lateral expansion of a landfill used for Coal Combustion Residuals (CCR) must comply with the following:

- Design, construct, operate, and maintain:
 - A run-on control system to prevent flow onto the active portion of the CCR unit during the peak discharge from a 24-hour, 25-year storm.
 - A run-off control system from the active portion of the CCR unit to collect and control at least the water volume resulting from a 24-hour, 25-year storm.
- Run-off from the active portion of the CCR unit must be handled in accordance with the associated surface water requirements.

- Prepare initial and periodic run-on and run-off control system plans for the CCR unit according to the following timeframes:
 - For existing CCR landfills, the owner or operator of the CCR unit must have prepared the initial run-on and run-off control system plan no later than October 17, 2016.
 - The owner or operator of the CCR unit must prepare periodic run-on and run-off control system plans every five (5) years thereafter.
- Obtain a certification from a qualified professional engineer stating that the initial and periodic run-on and run-off control system plans meet the requirements of this section.
- Comply with the recordkeeping requirements specified in 30 TAC 352.1301, the notification requirements specified in 30 TAC 352.1311, and the Publicly Accessible Website requirements specified in 30 TAC 352.1321.

This Run-on and Run-off Control System Plan presents the regulatory-required materials as noted above for the Welsh Ash Landfill. Though design of permanent runon and run-off control measures were prepared for the Welsh Ash Landfill in the previously submitted/approved Design Modification, this Run-on and Run-off Control System Plan addresses a combination of both interim and permanent systems which are hereafter described.

As the Welsh Ash Landfill is subsequently filled and completed, periodic updates to this Run-on and Run-off Control System Plan may be required.

2.0 Run-on Control Systems

Run-on Controls are provided and accomplished for the interim condition of the Welsh Ash Landfill by a combination of perimeter grading conditions and interim/permanent perimeter drainage systems. The design and function of these systems are as follows:

2.1 Perimeter Grading Conditions

As shown in Figure 1 – Fly Ash Storage Area Phase I (WEPX-88), the Welsh Ash Landfill was constructed with a screen dike on the entire west, north and east sides with drainage culverts located on the north and the southeast areas. A berm of minimal length was constructed on the eastern side of the south boundary. The net effect of this original construction is a perimeter grading condition that is an average of fifteen feet above the surrounding area. As a result of this perimeter grading condition and the hydraulic and hydrological conditions demonstrated in perimeter drainage systems hereafter, a run-on control system to prevent flow onto the active portion of the CCR unit during the peak discharge from a 24-hour, 25-year storm has been in place from the outset.

2.2 Interim & Permanent Perimeter Drainage Systems

As shown in Figure 2 – Current TCEQ NOR Site Development Plan, the future condition of the Welsh Ash Landfill provides for a perimeter drainage system consisting of varying depth perimeter drainage systems (ditches). These perimeter drainage systems are designed as both a run-on and run-off control system to prevent flow onto or away from the active portion of the landfill during the peak discharge from a 24-hour, 25-year storm (Design Event).

In the interim condition, as shown in Figure 3 – Composite Existing Conditions (Merged Field & LiDAR Topography) and the associated Figure 4 – Existing & Proposed Conditions - Drainage Area Map, interim/permanent perimeter drainage systems have been provided. Currently the Run-on and Run-off Control System includes permanent components of the perimeter drainage systems along a portion of the east and northeast sides of the Welsh Ash Landfill. All other perimeter drainage systems are interim. These perimeter ditches are designed to likewise prevent flow onto the active portion of the landfill during the peak discharge from the Design Event.

2.3 Summary of Design Requirements & Justifications

Both Table 1 – Drainage Area Summaries and Table 2 – Q25 Run-on and Run-off Analysis Justifications (and supporting design calculations), as contained in Appendix 2, provide a summary of hydraulic and hydrologic capacity of the interim run-on/run-off control system. These analyses demonstrate that, in all instances, the currently implemented (and maintained) drainage system functions to control run-on for the peak discharge from a 24-hour, 25-year storm.

3.0 Run-off Control Systems

Run-off Controls are provided and accomplished for the interim condition of the Welsh Ash Landfill by a combination of perimeter grading conditions and interim/permanent perimeter drainage systems. The design, operation and maintenance of these perimeter drainage systems provide for conveyance of all 24-hour, 25-year storm run-off from within the Welsh Landfill to the Primary Bottom Ash Pond, a management unit designed to accommodate these flows and other process discharges from the Welsh Power Plant. The design and function of these systems are as summarized follows:

3.1 Perimeter Grading Conditions

As previously noted, the original construction resulted in a perimeter grading condition that is an average of fifteen feet above the surrounding area. As a result of this perimeter grading condition and the hydraulic and hydrological conditions demonstrated in perimeter drainage systems hereafter, an uncontrolled run-off control system is in place to prevent flow away from the active portion of the CCR unit during the peak discharge from a 24-hour, 25-year storm.

3.2 Interim Top Slope Diversion Berms and Swales

Due to proximity to interim perimeter drainage systems, Drainage Areas CDA 01, CDA 02, CDA 03, CDA 04, and CDA 05 currently require drainage swales in conjunction with berms, dikes or other top slope diversions to ensure contact runoff is managed within the landfill. As shown in Figure 3 – Composite Existing Conditions (Merged Field & LiDAR Topography) and the associated Figure 4 – Existing & Proposed Conditions - Drainage Area Map, these drainage features are configured with the purpose of preventing run-off from the adjacent perimeter drainage areas during a 24-hour, 25-year storm event.

3.3 Permanent Side Slope Terraces and Letdowns

Currently the Run-on and Run-off Control System includes earthen side slope terraces and letdowns along a portion of the east and northeast sides of the Welsh Ash Landfill. The future side slopes of the landfill will extend at a 3H:1V slope to a height of approximately 75-feet above the flowline of the permanent perimeter drainage systems (ditch). These systems or similar will be extended as the landfill continues to fill.

In accordance with Figure 2 – Current TCEQ NOR Site Development Plan and associated design, these terraces and letdowns are designed and implemented as run-off control systems to accommodate runoff from a 24-hour, 25-year storm (Design Event), when needed.

3.4 Interim and Permanent Perimeter Drainage Systems

As shown in Figure 2 – Current TCEQ NOR Site Development Plan, the future condition of the Welsh Ash Landfill provides for a perimeter drainage system consisting of varying depth perimeter drainage systems (ditches). These perimeter ditches are designed as both a run-on and run-off control system to prevent flow onto or away from the active portion of the landfill during the peak discharge from a 24-hour, 25-year storm (Design Event).

In the interim condition, as shown in Figure 3 – Composite Existing Conditions (Merged Field & LiDAR Topography) and the associated Figure 4 – Existing & Proposed Conditions - Drainage Area Map, some of these perimeter drainage systems (ditches) have been provided. Currently the Run-on and Run-off Control System includes permanent components of the perimeter drainage systems along a portion of the north and east sides of the Welsh Ash Landfill. All other perimeter drainage systems are interim. These perimeter ditches are designed to likewise prevent flow onto the active portion of the landfill during the peak discharge from the Design Event.

3.5 Interim and Permanent Culvert Systems

3.5.1 Interim. Driveway crossings are implemented around the perimeter drainage system on an as-needed basis. These crossings are considered interim; however, are sized for run-on and run-off control for the Design Event.

3.5.2 Permanent Culvert Systems, designed to control run-on and run-off equal to or greater than the 24-hour, 25-year design storm event and conveying same to the Primary Bottom Ash Pond, are currently in place as follows:

- Two HDPE culverts, one 30-inches in diameter and one 36-inches in diameter, in the perimeter ditch at the northeast corner of the Welsh Ash Landfill;
- Two 30-inch diameter HDPE culverts in the perimeter ditch at the northwest corner of the Welsh Ash Landfill; and
- A series of three 30-inch diameter HDPE culverts collecting and discharging stormwater runoff from within the landfill at the original "Culvert Number 2" (shown as 2a, 2b, and 2c) location (future landfill leachate collection sump).

3.6 Permanent Low Water Crossing System

The run-on and run-off designs provide for run-off to be routed south via a low water crossing. This low water crossing is comprised of a textured reinforced concrete trapezoidal broadcrest section, 10-feet wide by 2.76' deep with 12H:1V side slopes and a -1.1% slope along the flowline. The crossing is sized and configured for in excess of the 24-hour, 25-year storm event for future landfill sideslope, terraces and letdowns.

At present, this low water crossing is blocked by perimeter berms to ensure that contact stormwater is routed to the Culvert Number 2 (shown as 2a, 2b, & 2c) location for discharge.

3.7 Summary of Design Requirements and Justifications

Both Table 1 – Drainage Area Summaries and Table 2 – Q25 Run-on and Run-off Analysis Justifications (and supporting design calculations), as contained in Appendix 2, provide a summary of hydraulic and hydrologic capacity of the interim run-on/run-off control system. These analyses demonstrate that, in all instances, the currently implemented (and maintained) drainage system function to control run-off for the peak discharge from a 24-hour, 25-year storm.

4.0 Summary of Requirements, Justifications and Conclusions

As previously stated,30 TAC 352.811 (and by reference Federal Regulation Title 40, Part 257.81) requires the owner or operator of an existing or new landfill or any lateral expansion of a landfill used for Coal Combustion Residuals (CCR) to comply with design, construction, operation, maintenance, certification and recordkeeping requirements that are summarized as follows:

- Design, construct, operate, and maintain:
 - A run-on control system to prevent flow onto the active portion of the CCR unit during the peak discharge from a 24-hour, 25-year storm.
 - A run-off control system from the active portion of the CCR unit to collect and control at least the water volume resulting from a 24-hour, 25-year storm.
- Run-off from the active portion of the CCR unit must be handled in accordance with the surface water requirements under 30 TAC 352.2.
- Prepare initial and periodic run-on and run-off control system plans for the CCR unit according to the following timeframes:
 - For existing CCR landfills, the owner or operator of the CCR unit must have prepared the initial run-on and run-off control system plan no later than October 17, 2016.
 - The owner or operator of the CCR unit must prepare periodic run-on and run-off control system plans every five (5) years thereafter.
- Obtain a certification from a qualified professional engineer stating that the initial and periodic run-on and run-off control system plans meet the requirements of this section.
- Comply with the recordkeeping requirements specified in 30 TAC 352.1310, the notification requirements specified in 30 TAC 352.1311, and the Publicly Accessible Website requirements specified in 30 TAC 352.1321.

Both Table 1 – Drainage Area Summaries and Table 2 – Q25 Run-on and Run-off Analysis Justifications (and supporting design calculations), as contained in Appendix 2, provide a summary of hydraulic and hydrologic capacity of the interim run-on/run-off control system. These analyses demonstrate that, in all instances, the currently implemented (and maintained) drainage system functions to control both run-off and run-on for the peak discharge from a 24-hour, 25-year storm.

5.0 Plan Review and Changes in Welsh Ash Landfill Configuration

Landfill Owner and/or Operator will review and evaluate this Plan every five (5) years from initial plan preparation and when there are changes in the facility design, construction, operation, or maintenance that materially affect the facility's potential for run-on and run-off control. Amendments to the Plan made to address changes of this nature are referred to as technical or major amendments and must be certified by a Professional Engineer. Non-technical amendments include the following:

Technical and administrative amendments to the Plan will be documented on the Plan Review Log. Owner/Operator will make the necessary revisions to the Plan as soon as possible, but no later than six months after the change occurs. The Plan must be implemented as soon as possible following a technical amendment, but no later than six months from the date of the amendment. The Designated Person is responsible for initiating and coordinating revisions to the Spill Prevention, Control, and Countermeasure (SPCC) Plan.

Scheduled reviews and Plan amendments will be recorded in the Plan Review Log provided in Appendix 3. The log will be completed even if no amendment is made to the Plan as a result of the review.

6.0 Professional Engineer Certification

The original plan and all reviews and amended plans must obtain certification from a qualified professional engineer stating that the initial and periodic run-on and run-off control system plans meet the requirements of TAC 352.811 (and by reference 40 CFR 257.81). This certification in no way relieves the owner or operator of the facility of his/her duty to fully implement this Plan. The Professional Engineer Certification page is provided in Appendix 4.

Appendix 1: Figures

- Figure 1 Fly Ash Storage Area Phase I (WEPX-88)
- Figure 2 Current TCEQ NOR Site Development Plan
- Figure 3 Composite Existing Conditions (Merged Field & LiDAR Topography)
- Figure 4 Existing & Proposed Conditions Drainage Area Map

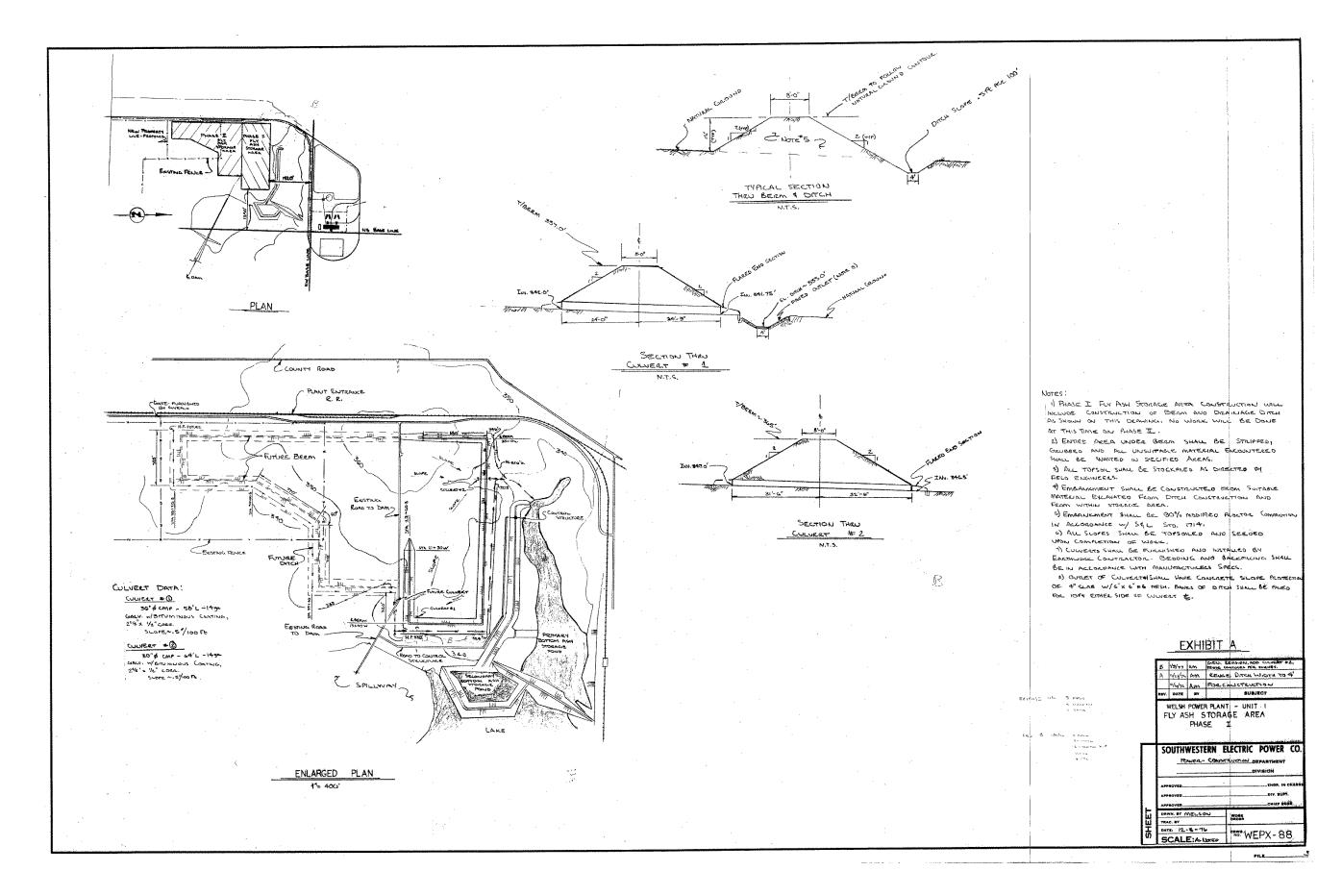


Figure 1- Fly Ash Storage Area Phase I (WEPX-88)

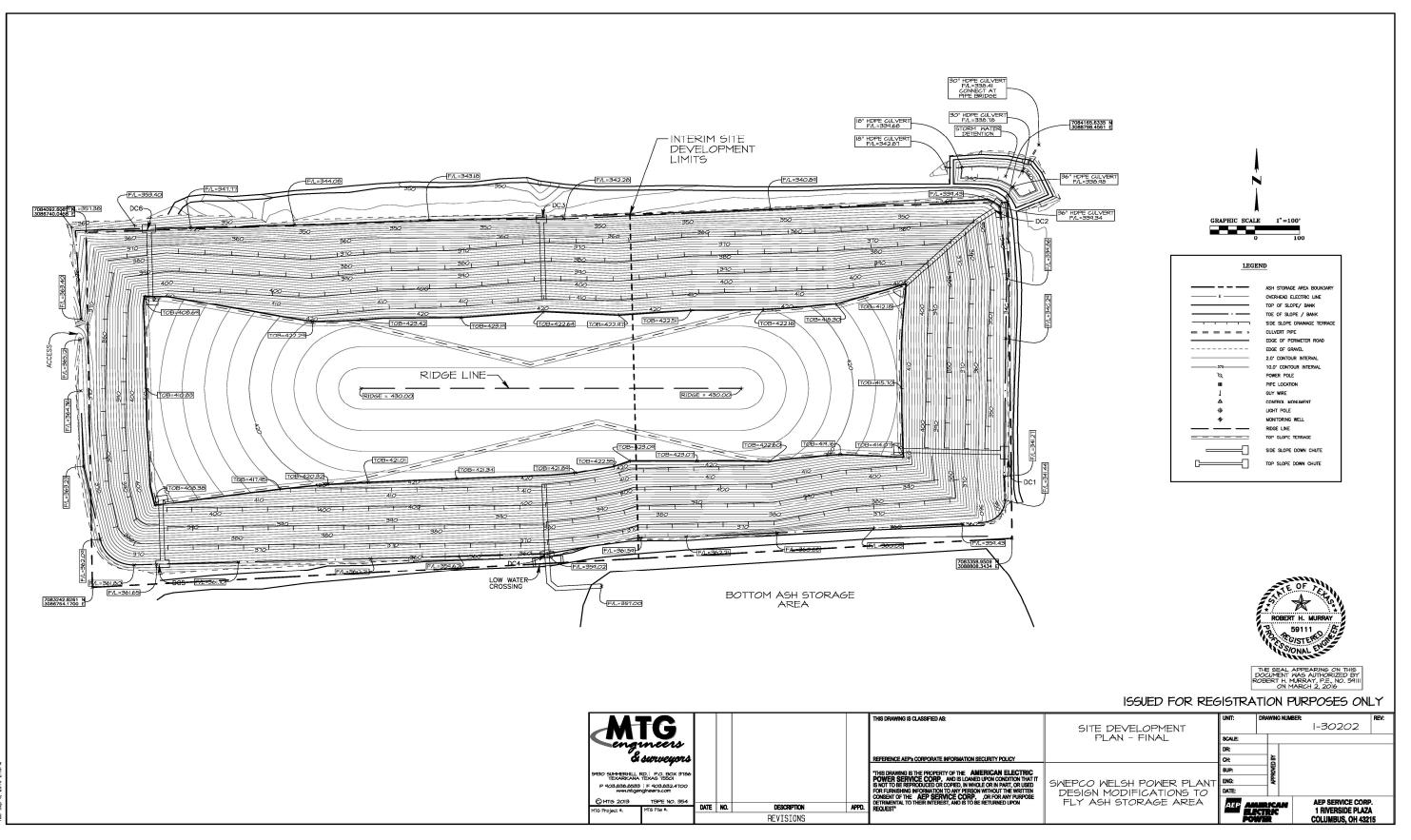


Figure 2 - Current TCEQ NOR Site Development Plan

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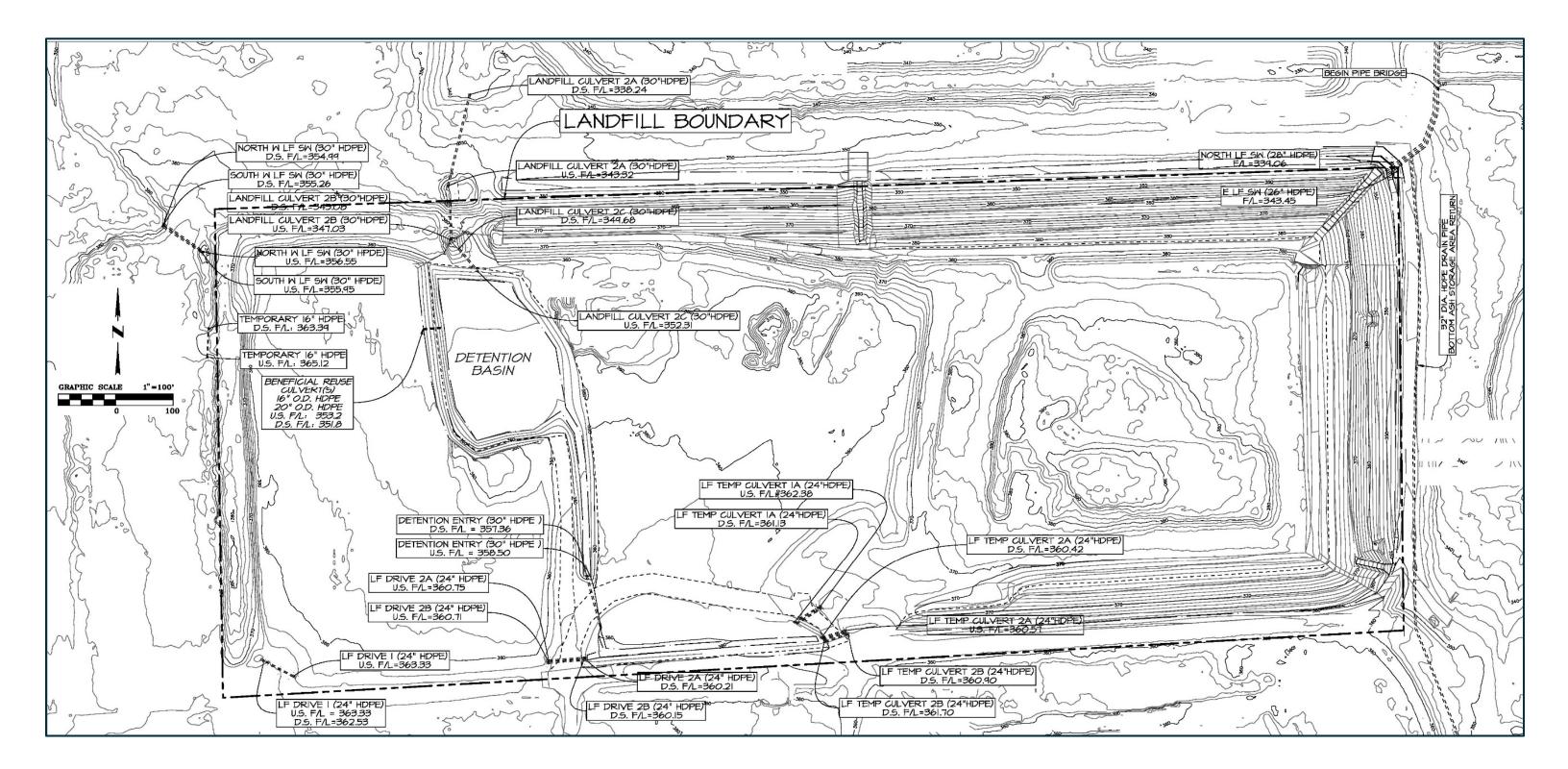


Figure 3 - Composite Existing Conditions (Merged Field & LiDAR Topography)

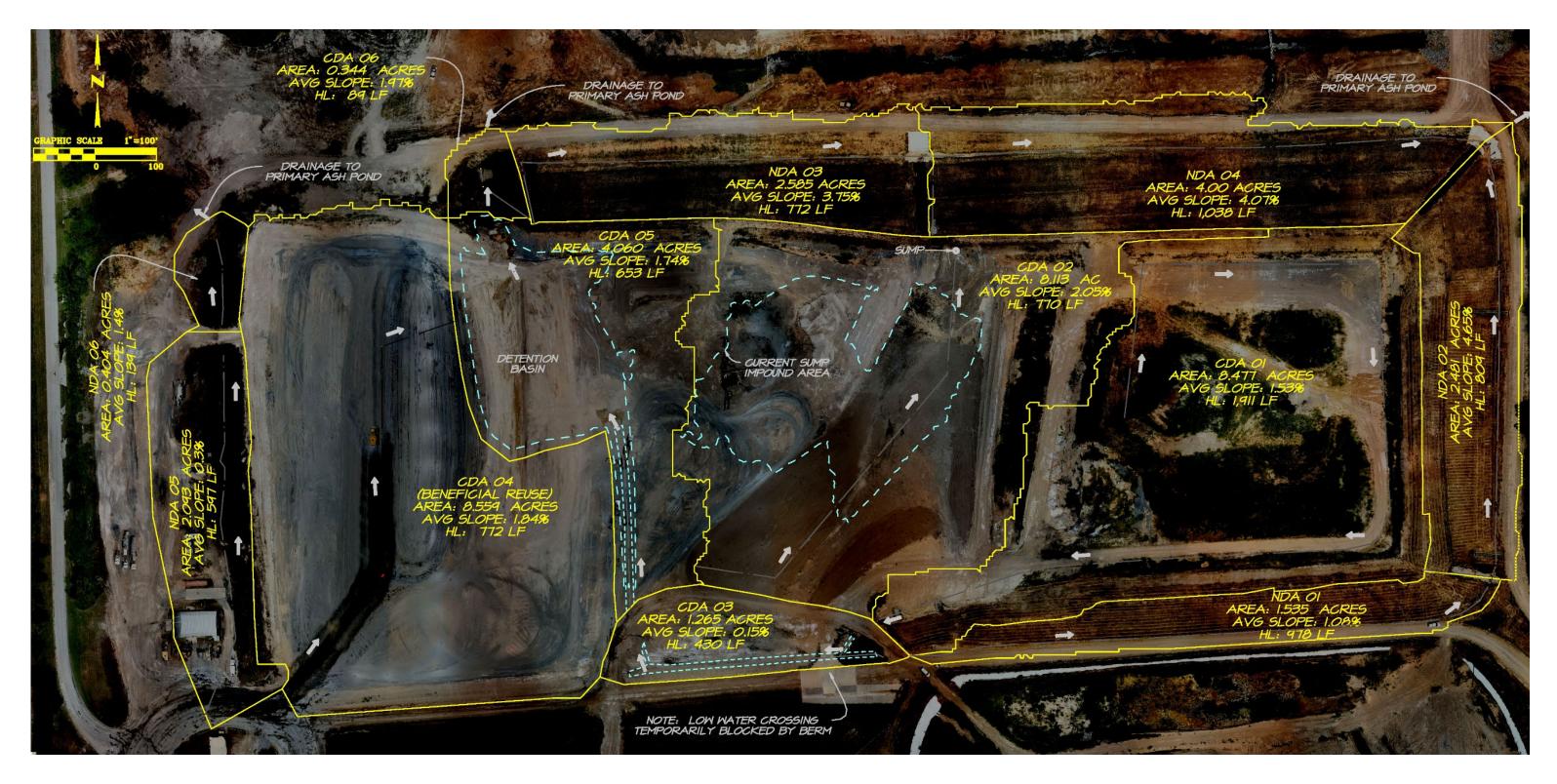


Figure 4 – Existing & Proposed Conditions - Drainage Area Map

Appendix 2: Tables

- Table 1 Drainage Area Summaries
- Table 2 Q25 Run-on and Run-off Analysis Justifications

DRAINAGE AREA SUMMARIES												
					HYDRAULIC		CALCULATED	USED				
DRAINAGE	DISCHARGE		AREA	SLOPE	LENGTH	RATIONAL	тс	тс				
AREA ID	STATUS	DRAINAGE AREA LOCATION	(ACRES)	(%)	(FEET)	C FACTOR	(MIN)	(MIN)				
CDA 01	CONTACT	LANDFILL INTERIOR	8.477	1.53%	1911	0.40	13.00	13.00				
CDA 02 *	CONTACT	LANDFILL INTERIOR	8.113	2.05%	770	0.50	5.85	10.00				
CDA 03	CONTACT	LANDFILL INTERIOR	1.265	0.15%	430	0.50	10.74	11.00				
CDA 04	CONTACT	LANDFILL INTERIOR	8.559	1.84%	772	0.50	6.08	10.00				
CDA 05 **	CONTACT	LANDFILL INTERIOR	4.060	1.74%	653	0.50	5.76	10.00				
CDA 06	CONTACT	LANDFILL INTERIOR	0.344	1.97%	89	0.75	1.12	10.00				
NDA 01	NON-CONTACT	LANDFILL PERIMETER DITCH	1.535	1.08%	978	0.50	8.95	10.00				
NDA 02	NON-CONTACT	LANDFILL PERIMETER DITCH	2.481	4.65%	809	0.50	4.41	10.00				
NDA 03	NON-CONTACT	LANDFILL PERIMETER DITCH	2.585	3.75%	772	0.50	4.32	10.00				
NDA 04	NON-CONTACT	LANDFILL PERIMETER DITCH	4.000	4.07%	1038	0.50	5.62	10.00				
NDA 05	NON-CONTACT	LANDFILL PERIMETER DITCH	2.093	0.30%	597	0.40	10.02	10.00				
NDA 06	NON-CONTACT	LANDFILL PERIMETER DITCH	0.404	1.40%	139	0.40	1.80	10.00				
	* Q25 DISCHARGE IS BY LEA	ACHATE COLLECTION SUMP PUMP AT 30 GPM (0.08	027 CFS)	* Q25 DISCHARGE IS BY LEACHATE COLLECTION SUMP PUMP AT 30 GPM (0.08027 CFS)								

Table 1 – Drainage Area Summaries

Q-25 RUN-ON/RUN-OFF ANALYSIS JUSTIFICATIONS													
				ANALYSIS	ANALYSIS	BASIN	HYDRAULIC		ANALYSIS	REQUIRED		AVAILABLE	ANALYSIS
ANALYSIS	JUSTIFICATION ANALYSIS	DRAINAGE		AREA	SLOPE	SLOPE	LENGTH	ANALYSIS	тс	Q25 CAPACITY	ANALYSIS JUSTIFICATION	DEPTH	DEPTH
ID	DRAINAGE AREAS INCLUDED	STATUS	ANALYSIS TYPE	(ACRES)	(%)	(%)	(FEET)	C FACTOR	(MIN)	(CFS)	CONFIGURATION	(FT)	(FT)
TERNAL CON	TACT DRAINAGE AREAS												
I-01	CDA 01	CONTACT	TWO 24" HDPE CULVERTS	8.477	0.86%	1.53%	1911	0.40	13.00	27.09	TWO 52-FT LONG X 24" DIA HDPE CULVERTS	4.90	4.19
1-02	CDA 02 (LEACHATE COLLECTION AREA)	CONTACT	DRAINAGE CAPTURED & REMOVED	8.113	2.05%	2.05%	770	0.50	10.00	36.27	AREA RETAINS Q-25 RUNOFF VIA DETENTION	2.38	1.93
			BY SUMP PUMP								PEAK Q = 0.07 CFS		
I-03	CDA 01 & CDA 03	CONTACT	TRAPEZOIDAL CHANNEL, 3:1 SIDES	9.742	0.15%	1.35%	2341	0.41	23.74	23.32	0.15% 10-FT CHANNEL, 3:1 Sides, 1.5-FT DEEP	1.50	0.54
	CDA 01 & CDA 03	CONTACT	TWO 60'X24" HDPE CULVERTS	9.742	2.33%	1.35%	2341	0.41	23.74	23.32	70-FT LONG X 30" DIA HDPE CULVERT	8.80	2.51
1-04	CDA 04	CONTACT	TWO 32'X16" HDPE CULVERTS	8.559	4,37%	1.84%	772	0.50	10.00	38.26	TWO 32-FT LONG X 16" DIA HDPE CULVERTS *	6.22	6.92
104		continer		0.000	10770	210475	,,,	0100	10100	50120		0122	0132
1-05	DETENTION - AREAS CDA 1, 3, 4 & 5	CONTACT	DETENTION BASIN TO SERIES OF HDPE PIPES	22.361	4.35%	1.26%	2994	0.57	20.00	82.21	SERIES - TWO 30" HDPE CULVERTS - PEAK Q = 34.74 CFS	8.00	3.29
1-05	DETENTION - AREAS CDA 1, 3, 4 & 5	CONTACT	DETENTION DASIN TO SERIES OF TIDPE FIFES	22.501	4,5576	1.20%	2354	0.57	20.00	02.21	SERIES - 1990 50 HIDEL COLVERTS - PEAK Q - 34.74 CT3	8.00	3.23
1-06	DETENTION I-05 DISCHARGE	CONTACT	32'X32" HDPE CULVERT	22.705	0.40%	1.26%	3083	0.57	N/A	34.74	USE I-05 DETENTION PEAK DISCHARGE	8.00	3.27
		CONTACT	SZ XSZ HDPE CULVERT	22.705	0.40%	1.20%	5085	0.57	N/A	54.74	USE 1-05 DETENTION PEAK DISCHARGE	8.00	3.27
	N-CONTACT DRAINAGE AREAS			1 525	0.20%	1.07%	070	0.50	10.00	6.0		1.80	1 1 2
P-01	NDA 01	NON-CONTACT	V-DITCH, 3:1 SIDES	1.535	0.30%	1.97%	978	0.50	10.00	6.9	0.3% V-DITCH, 3:1 SIDES, 1.78-FEET DEPTH	1.80	1.13
5.03				1.016	0.00%	2 20%	4707	0.50	40.00	47.07		4.00	4.62
P-02	NDA 01 & NDA 02	NON-CONTACT	5' CHANNEL, 3:1 SIDES	4.016	0.30%	3.29%	1787	0.50	10.00	17.97	0.3% - V-DITCH, 3:1 SIDES, 4-FEET DEPTH	4.00	1.63
P-03	NDA 03	NON-CONTACT	20' CHANNEL, 3:1 SIDES	2.585	0.30%	10.05%	772	0.50	10.00	11.56	0.3% - 20' CHANNEL, 3:1 SIDES, 7.5-FEET DEPTH	7.70	0.39
P-04	NDA 03 & NDA 04	NON-CONTACT	15' CHANNEL, 3:1 SIDES	6.585	0.30%	3.94%	1810	0.50	10.00	29.46	0.3% - 15' CHANNEL, 3:1 SIDES, 6.5-FEET DEPTH	6.50	0.80
P-02 & P04	DETENTION - AREAS NDA 01, 02,03 & 04	NON-CONTACT	426'X26" HDPE, U.S. 343.45, D.S. 335.48	10.601	1.87%	3.69%	1810	0.5	10.00	47.38	426'X26' HDPE @ 1.887% (COMBINED MAX Q = 38.49 CFS)	4.05	N/A
		NON-CONTACT	587'X28" HDPE, U.S. 339.06, D.S. 333.87		0.88%						587X28' HDPE @ 0.88%	8.44	2.42
P-05	NDA 05	NON-CONTACT	.3% V-DITCH, 3:1 L & 4:1R SIDES	2.093	3.46%	0.30%	597	0.4	10.00	7.49	.3% V-DITCH, 3:1 L & 4:1R SIDES	4.60	1.10
			50'X16" TEMP HDPE, U.S.365.12, D.S. 363.39								50'X16" TEMP HDPE @ 3.46%	6.72	1.92
P-06	NDA 05 & NDA 06	NON-CONTACT	.3% V-DITCH, 3:1 L & 3:1R SIDES	2.497	1.19%	1.19%	736	0.40	10.00	8.94	.3% V-DITCH, 3:1 L & 3:1R SIDES	1.92	1.73
			TWO 84'X30" HDPE, U.S.356.55, D.S. 355.26	2.497	1.54%	1.19%	736	0.40	10.00	8.94	TWO 84'X30" HDPE, U.S.356.55, D.S. 355.26	8.20	0.99

Table 2 - Q25 Run-on and Run-off Analysis Justifications

ANALYSIS JUSTIFICATION CALCULATIONS INTERNAL CONTACT DRAINAGE AREAS

Note: "Contact Drainage Areas" refers to storm water runoff from these areas having come in contact with CCR materials.

ANALYSIS JUSTIFICATION - SECTION I-01

PROJECT: Welsh Run-On & Run-Off Protection Plan\2021 DA Map with H&H Calcs.pro _____ HYDROLOGIC REPORT _____ DEVELOPED UNIVERSAL RATIONAL HYDROGRAPH O(PEAK) = C*I*A25 YEAR STORM FREQUENCY BASIN IDENTIFIER SECTION I-01 (CDA 01) DISCHARGES INTO WELSH ASH LANDFILL BASIN AREA = 8.48 ACRES RUNOFF COEFF. = 0.40 RAINFALL INT. = 7.99 IN/HR TIME OF CONC. = 13.00 MINUTES TIME RUNOFF (CFS) (MIN) -----_____ 0.0 0.0 6.5 13.5 13.0 27.1 I-01 19.5 18.9 30 г WELSH ASH LANDFILL 10.8 26.0 DEVELOPED 27 32.5 8.8 25 YEAR STORM 6.8 MAX Q = 27.09 cfs VOLUME = 50148.5 cu ft 39.0 24 45.5 5.9 52.0 4.9 21 58.5 4.4 65.0 3.9 18 (cfs) 71.5 3.6 15 Runoff 78.0 3.2 84.5 3.1 12 91.0 2.9 97.5 2.7 g 104.0 2.4 110.5 2.4 117.0 2.3 3 123.5 1.1 130.0 0.0 57 76 95 114 133 152 171 38 190 Time (minutes) 136.5 0.0 143.0 0.0 149.5 0.0 0.0 156.0 162.5 0.0 169.0 0.0 175.5 0.0 182.0 0.0 188.5 0.0
 PEAK FLOW =
 27.09
 CFS

 TIME TO PEAK =
 13.00
 MIN
 TOTAL VOLUME = 50148.54 CU FT

I-01 CULVERTS: <u>TWO 52' X 24" DIA HDPE CULVERTS, 4.9' MAX HW DEPTH</u> 4.19' CALCULATED HW DEPTH - MEETS Q-25 REQUIREMENT*

Solve For: He	eadwater El	evation	•			
Culvert				Inverts		
	Discharge:	27.09	cfs	Invert Upstream:	362.40	ft
Maximum Allo	wable HW:	367.30	ft	Invert Downstream:	361.13	ft
Tailwater	r Elevation:	0.00	ft	Length:	52.00	ft
Section				Slope:	0.024423	ft/ft
Shape:	Circular		•	- Headwater Elevation	ons	
Material:	Corrugated	HDPE (Smooth In	•	Maximum Allowab	ole: 367.30	ft
Size:	24 inch		•	Computed Headwat	er: 364.43	ft
Number:	2			Inlet Contr	rol: 364.34	ft
Mannings:	0.012		•	Outlet Contr	rol: 364.43	ft
- Inlet				Exit Results		
Entrance:	Beveled ring	g, 33.7° bevels	•	Discharge: 27.0	9	cfs
Ke:	0.20			Velocity: 10.0	8	ft/s
				Depth: 0.89		ft

* Bentley CulvertMaster – Culvert Analysis

ANALYSIS JUSTIFICATION - SECTION I-02

PROJECT: Welsh			ection Plan\2021		
HYDROLOGIC REPOR	RT				
DEVELOPED UNIVER Q(PEAK) = C*I*A 25 YEAR STORM FI BASIN IDENTIFIER	REQUENCY	L HYDROGRA	РН		
DISCHARGES INTO		H LANDFILI			
BASIN AREA =	8.11	ACRES			
RUNOFF COEFF. =	0.50				
RAINFALL INT. = TIME OF CONC. =	8.94	IN/HR			
		MINUTES			
	RUNOFF				
	(CFS)				
0.0	0.0				
5.0	18.1				
10.0	36.3				
15.0	26.2				
20.0	16.1 13.1	40 г			CDA 02
25.0 30.0	10.2				WELSH ASH LANDFILL
	8.9	э6 -	1		DEVELOPED 25 YEAR STORM
	7.5		Λ		MAX Q = 36.27 cfs Volume = 55419.9 cu ft
	6.8	32 -	Λ		
	6.0		(Λ)		
55.0	5.5	28 -	1 \		
60.0	5.0		1 \		
65.0	4.6	24 - ĵo			
70.0	4.1	- 02 + (cfs)			
75.0	3.9	+ 20 - 1 gang			
80.0	3.7	ح 16 -			
	3.6		\backslash		
90.0	3.4	12 -	\backslash		
95.0	1.7	1			
100.0	0.0	8-			
105.0	0.0				
110.0	0.0	4			
115.0 120.0	0.0 0.0		<u> </u>	· · · · · · · · · · · · · · · · · · ·	
125.0	0.0	90	15 30 45 6	50 75 90 Time (minutes)	105 120 135 150
130.0	0.0				
135.0	0.0				
140.0	0.0				
145.0	0.0				
<mark>PEAK FLOW =</mark>		7 CFS			
TIME TO PEAK =					
TOTAL VOLUME =	<mark>= 55419.9</mark>	<mark>0 CU FT</mark>			

NOTE: Section I-02 is essentially a leachate collection cell which drains to the north side of the landfill where water is collected in a sump and pumped to the Primary Ash Pond return system. As a result, Section I-02 does not discharge to the stormwater run-on & run-off system and is treated as a detention pond with no Q25 impact to landfill drainage systems.

ANALYSIS JUSTIFICATION - SECTION I-02 (CONT)

_____ HYDROLOGIC REPORT - STAGE, STORAGE, AND DISCHARGE Pumped Detention Area - CDA 02 _____ 1=USER DEFINED 1) 356.620 Q 0.00 Through 7) 359.500 Q 0.07 STORAGE OUTFLOW (CU.FT.) (CFS) 2S/T+O (CFS) ELEV (CFS) _____

 356.62
 0.0

 356.67
 0.0

 356.72
 0.0

 356.76
 0.0

 356.81
 0.0

 356.91
 0.0

 356.95
 0.0

 357.00
 0.0

 357.13
 137.0

 357.19
 205.5

 0.1 0.5 0.1 1.0 205.5 274.1 0.1 357.19 1.4 357.25274.1357.31342.6357.38411.1357.44479.6357.50548.1357.631282.5357.691649.7357.752016.9357.812384.1357.943118.5358.003485.7358.135563.4 0.1 1.9 357.25 2.4 2.8 3.3 3.7 6.2 8.6 11.1 13.5 16.0 18.4 0.1 0.1 20.9 0.1 23.3 30.2 0.1 5563.4 0.1 37.2 358.13 358.135563.4358.196602.2358.257641.0358.318679.8358.389718.7358.4410757.5358.5011796.3358.5613968.8358.6316141.3358.6918313.8358.7520486.3358.8122658.7 0.1 44.1 0.1 51.0 57.9 0.1 0.1 64.9 0.1 71.8 0.1 78.7
 0.1
 93.2

 0.1
 107.7

 0.1
 122.2

 1
 136.6
 136.6 0.1 358.81 22658.7 0.1 151.1 358.8824831.2358.9427003.7359.0029176.2 0.1 0.1 165.6 180.1 194.6 0.1

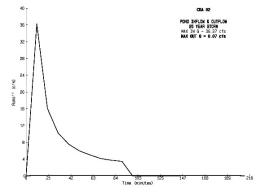
PROJECT: Welsh Run-On & Run-Off Protection Plan\2021 DA Map with H&H Calcs.pro

ANALYSIS JUSTIFICATION - SECTION I-02 (CONT)

PROJECT: Welsh Run-On & Run-Off Protection Plan\2021 DA Map with H&H Calcs.pro

SECTION	I-02	HYDROGRAPH	ROUTING	(Disch	arges via	Forcemain	to Primary	
PUMPED I	DETENT	ION AREA:	CDA 02					
Т	I1	ION AREA:	2S1/T	01	2S2/T+O2	02	2S2/T	
25 YEAR	STORM	FREQUENCY						
5.00	0.0	FREQUENCY 18.1 36.3 26.2	0.0	0.0	18.1	0.1	18.1	
10.00	18.1	36.3	18.1	0.1	72.4	0.1	72.3	
15.00	36.3	26.2	72.3	0.1	134.7	0.1	134.6	
20.00	26.2	16.1 13.1 10.2	134.6	0.1	176.8	0.1	176.7	
25.00	16.1	13.1	176.7	0.1	205.9	0.1	205.8	
30.00	13.1	10.2	205.8	0.1	229.1	0.1	229.0	
35.00	10.2	8.9	229.0	0.1	248.1	0.1	248.0	
40.00	8.9	7.5 6.8 6.0	248.0	0.1	264.4	0.1	264.3	
45.00	7.5	6.8	264.3	0.1	278.5	0.1	278.5	
50.00	6.8	6.0	278.5	0.1	291.1	0.1	291.0	
55.00	6.0	5.5	291.0	0.1	302.4	0.1	302.3	
60.00	5.5	5.5 5.0 4.6	302.3	0.1	312.7	0.1	312.7	
65.00	5.0	4.6	312.7	0.1	322.2	0.1	322.1	
70.00	4.6	4.1	322.1	0.1	330.7	0.1	330.7	
75.00	4.1	3.9	330.7	0.1	338.7	0.1	338.6	
80.00	3.9	3.9 3.7	338.6	0.1	346.2	0.1	346.1	
85.00	3.7	3.6	346.1	0.1	353.4	0.1	353.3	
90.00	3.6	3.4 1.7 0.0	353.3	0.1	360.3	0.1	360.2	
95.00	3.4	1.7	360.2	0.1	365.3	0.1	365.3	
100.00	1.7	0.0	365.3	0.1	366.9	0.1	366.9	
105.00	0.0	0.0	366.9	0.1	366.8	0.1	366.7	
110.00	0.0	0.0	366.7	0.1	366.7	0.1	366.6	
115.00	0.0 0.0 0.0	0.0 0.0 0.0	366.6	0.1	366.5	0.1	366.5	
	0.0	0.0	366.5	0.1	366.4	0.1	366.3	
125.00	0.0	0.0	366.3	0.1	366.2	0.1	366.2	
130.00	0.0	0.0	366.2	0.1	366.1	0.1	366.0	
135.00	0.0	0.0	366.0	0.1	366.0	0.1	365.9	
140.00	0.0	0.0	365.9	0.1	365.8	0.1	365.8	
145.00	0.0	0.0	365.8	0 1	365 7	0 1	365.6	
150.00	0.0	0.0 0.0 0.0	365 6	0.1	365 6	0 1	365.5	
155.00	0.0	0.0	365 5	0.1	365 4	0 1	365.4	
160.00	0.0 0.0 0.0	0.0 0.0 0.0	365 4	0.1	365 3	0 1	365.2	
165.00	0.0	0.0	365 2	0.1	365 2	0 1	365.1	
170.00	0.0	0.0	365 1	0.1	365 0	0 1	365.0	
175.00	0.0	0.0 0.0 0.0	365 0	0.1	361 9	0.1	364.8	
180.00	0.0	0.0	364 8	0.1	364.9	0.1	364.7	
185.00	0.0	0.0	364.0	0.1	364.6	0.1	364.6	
190.00	0.0	0.0	364.6	0.1	364.0	0.1	364.0	
195.00	0.0	0.0	364.0	0.1	364.4	0.1	364.3	
200.00	0.0	0.0	364.4	0.1	364.4	0.1	364.2	
200.00		0.0 ME TO PEAK		0.1	HOURS	U • 1	JU7.2	
		UM OUTFLOW		0.08	CFS			
		UM STORAGE		55028	CU FT	40 -		CDA 02
247		ELEVATION		65.41		эв - <mark>А</mark>		POND INFLOW & DUTFLOW 25 Year Storm Max in Q = 36.27 cfs
M					FT CIL ET	32 -		MAX OUT Q = 0.07 cfs
	INF.	LOW VOLUME	=	55420	CU FT			
		LOW VOLUME		804	CU FT	28 -		

MEETS Q25 REQUIREMENT (empties over time)



ANALYSIS JUSTIFICATION - SECTION I-03

		-Off Protection Plan\2021 DA Map with H&H Calcs.pro
DEVELOPED UNIV Q(PEAK) = C*I* 25 YEAR STORM :	ERSAL RATIONAL A	
BASIN IDENTIFI	ER I-03 (CDA	01 & CDA 03)
	= 9.74 A = 0.41 = 5.84 II = 24.00 M RUNOFF	CRES N/HR
(MIN)	(CFS)	
0.0 12.0 24.0 36.0 48.0 60.0 72.0 84.0 96.0 108.0 120.0	0.0 11.7 23.3 15.4 7.4 6.0 4.5 3.9 3.4 3.0 2.7	30 I-03 (CDA 01 & CDA 03) 27 WELSH ASH LANDFILL 27 DEVELOPED 25 YEAR STORM MAX Q = 23.32 cfs
120.0 132.0 144.0 156.0 168.0 180.0 192.0 204.0 216.0 228.0	2.7 2.4 2.1 2.0 2.0 1.8 1.7 1.6 1.4 0.7	VOLUME = 69922.8 cu ft
240.0 252.0 264.0 276.0 288.0 300.0 312.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	6 3 0 3 5 70 105 140 175 210 245 280 315 350 Time (minutes)
324.0 336.0 348.0	0.0 0.0 0.0	
PEAK FLOW		CFS
TIME TO PEAK TOTAL VOLUME	= 24.00	MIN

ANALYSIS JUSTIFICATION - SECTION I-03 (CONT)

I-03 CHANNEL: 0.15% V-DITCH, 10-FT TRAPEZOIDAL, 3:1 SIDES, 1.5-FT MIN. DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE) 0.55'CALCULATED DEPTH, MEETS Q-25 REQUIREMENT*

Solve For: Normal Depth	~	e	Friction Method: Mannin	ng Formula	~
Roughness Coefficient	0.030]	Flow Area:	6.3	ft²
Channel Slope:	0.015	ft/ft	Wetted Perimeter:	13.4	ft
Normal Depth:	6.5	in	Hydraulic Radius:	5.7	in
Left Side Slope:	3.000	H:V	Top Width:	13.27	ft
Right Side Slope:	3.000	H:V	Critical Depth:	6.3	in
Bottom Width:	10.00	ft	Critical Slope:	0.017	ft/ft
Discharge:	23.32	cfs	Velocity:	3.68	ft/s
			Velocity Head:	0.21	ft
			Specific Energy:	0.76	ft
			Froude Number:	0.938	
			Flow Type:	Subcritical	
1			1		

* Bentley FlowMaster V8i – Trapezoidal Channel Analysis

I-03 CULVERT: 70' X 30" DIA HDPE CULVERT, 8.8' MAX HW DEPTH 2.51' CALCULATED HW DEPTH - MEETS Q-25 REQUIREMENT*

Solve For: He	eadwater Elevation	•			
Culvert			Inverts		
	Discharge: 23.32	cfs	Invert Upstream:	358.50	ft
Maximum Allo	wable HW: 367.30	ft	Invert Downstream:	357.36	ft
Tailwater	r Elevation: 0.00	ft	Length:	70.00	ft
Section			Slope:	0.016286	ft/ft
Shape:	Circular	•	Headwater Elevation	ons	
Material:	Corrugated HDPE (Smooth In	•	Maximum Allowab	le: 367.30	ft
Size:	30 inch	•	Computed Headwat	er: 361.01	ft
Number:	1		Inlet Contr	rol: 360.92	ft
Mannings:	0.012	•	Outlet Contr	rol: 361.01	ft
- Inlet			Exit Results		
Entrance:	Beveled ring, 33.7° bevels	-	Discharge: 23.3	2	cfs
Ke:	0.20		Velocity: 10.1	5	ft/s
,			Depth: 1.19		ft

* Bentley CulvertMaster – Culvert Analysis

ANALYSIS JUSTIFICATION - SECTION I-05

	un-Off Protection Plan\2021 DA Map with H&H Calcs.pro
HYDROLOGIC REPORT	
DEVELOPED UNIVERSAL RATION Q(PEAK) = C*I*A 25 YEAR STORM FREQUENCY	
DISCHARGES INTO WELSH A BASIN AREA = 8.56 RUNOFF COEFF. = 0.50 RAINFALL INT. = 8.94 TIME OF CONC. = 10.00 TIME RUNOFF (MIN) (CFS)	ACRES IN/HR
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
40.0 8.0 45.0 7.1 50.0 6.3 55.0 5.8 60.0 5.3 65.0 4.8 70.0 4.4 75.0 3.9	40 I-04 (CDA 04) 36 WELSH ASH LANDFILL 36 DEVELOPED 32 25 YEAR STORM 32 MAX Q = 38.26 cfs 28 VOLUME = 58466.4 cu ft
85.03.890.03.695.01.8100.00.0105.00.0110.00.0115.00.0120.00.0125.00.0	$\frac{3}{12}$ 20 $\frac{16}{12}$ 16 12 $\frac{1}{12}$ $\frac{1}{15}$ 30 45 60 75 90 105 120 135 150 Time (minutes)
130.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 38. TIME TO PEAK = 10. TOTAL VOLUME = 58466.	00 MIN

ANALYSIS JUSTIFICATION - SECTION I-04 (CONT)

I-03 TEMPORARY CULVERTS: <u>TWO 32'X16" HDPE CULVERTS, 6.22' MAX HW DEPTH</u> 6.92' HW DEPTH (FOR 15" DIA CULVERTS) EXCEEDS (0.7') TOP OF ROCK BERM OF THE DETENTION BASIN; HOWEVER, FLOWS ARE CONTAINED MEETS Q-25 REQUIREMENT*

Solve For: H	eadwater Elevation	•			
Culvert			Inverts		
	Discharge: 38.26	cfs	Invert Upstream:	353.20	ft
Maximum Allo	wable HW: 359.42	ft	Invert Downstream:	351.80	ft
Tailwate	r Elevation: 0.00	ft	Length:	32.00	ft
Section			Slope:	0.043750	ft/ft
Shape:	Circular	•	Headwater Elevation	ons	
Material:	Corrugated HDPE (Smooth	In 💌	Maximum Allowab	le: 359.42	ft
Size:	15 inch	•	Computed Headwat	er: 360.12	ft
Number:	2		Inlet Contr	rol: 360.12	ft
Mannings:	0.012	•	Outlet Contr	ol: 359.97	ft
- Inlet			Exit Results		
Entrance:	Beveled ring, 33.7° bevels	•	Discharge: 38.2	6	cfs
Ke:	0.20		Velocity: 15.6	0	ft/s
,			Depth: 1.24		ft

Bentley CulvertMaster – Culvert Analysis - (Calculated W/ 15" Dia Culverts)

ANALYSIS JUSTIFICATION - SECTION I-05 SERIES OF TWO 30-IN DIA HDPE CULVERTS – DETENTION OUTLET

PROJECT: Welsh Run-On & Run-	Off Protection Plan\2021	
HYDROLOGIC REPORT		
DEVELOPED UNIVERSAL RATIONAL Q(PEAK) = C*I*A 25 YEAR STORM FREQUENCY BASIN IDENTIFIER I-05 (DETE DISCHARGES INTO WELSH ASH BASIN AREA = 22.36 AC RUNOFF COEFF. = 0.57 RAINFALL INT. = 6.45 IN TIME OF CONC. = 20.00 MI TIME RUNOFF (MIN) (CFS)	NTION FOR CDA 01, 03, 04 LANDFILL RES I/HR	<u>&</u> 05)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	81 -	(CDA 01, 03, 04 & 05) WELSH ASH LANDFILL DEVELOPED 25 YEAR STORM MAX Q = 82.21 cfs LUME = 213355.2 cu ft
180.0 6.2 190.0 3.1 200.0 0.0 210.0 0.0 220.0 0.0 230.0 0.0 240.0 0.0 250.0 0.0 260.0 0.0 270.0 0.0 290.0 0.0 PEAK FLOW = 82.21 TIME TO PEAK = 20.00 TOTAL VOLUME = 213355.20	CFS MIN CU FT	145 174 203 232 261 290 ne (minutes)

ANALYSIS JUSTIFICATION - SECTION I-05 (CONT) SERIES OF 30-IN DIA HDPE – DETENTION OUTLET

		n-On & Run-Ofi				H&H Calcs.pr
HYDROLOG	IC REPORT -	- STAGE, STOR	AGE, AND DI	SCHARGE		
		ION FOR CDA 0				
l=USER DEF	'INED *			10)	353.450	Q 30.00
1)	350.500	Q 0.00		11)	353.990	Q 38.00
2)	351.150	Q 2.00 Q 4.00		12)	354.470 355.040	Q 44.00
3)	351.440	Q 4.00		13)	355.040	Q 50.00
4)	351.660	Q 6.00		14)	355.910 356.650	Q 58.00
5)	351.860	Q 8.00		15)	356.650	Q 64.00
6)	352.040	Q 10.00		16)	357.180 358.040	Q 68.00
7)				17)	358.040	Q 74.00
8)	352.920	Q 22.00		18)	358.970	Q 80.00
9)	353.060	Q 16.00 Q 22.00 Q 24.00 OUTFLOW				
ELEV	STORAGE	OUTFLOW (CFS)	2S/T+0			
	(CU.FT.)	(CFS)	(CFS)			
350.50	0.0	0.0	0.0			
350.75			0.8		Discharge	(cfs) HW Elev. (ft)
351.00			1.6			0.00 350.50
351.25	615 8	2 7	4.7			2.00 351.15
351.50		4.5	8.6			4.00 351.44
351.75	3435.9	6.9	18.4			6.00 351.66
352.00	5665.9	9.6	28.4			8.00 351.86
352.25	10391.0	12.7	47.4			0.00 352.04
352.50	15116.1	12.7 16.0	66.4			
352.75	22732.0	19.6	95.3			2.00 352.20
353.00	30347.8		124.3			4.00 352.35
353.25	40426.1		161.7			6.00 352.50
353.50	50504.3		199.1			8.00 352.65
353.75	62132.0		241.6			0.00 352.78
354.00	73759.7		284.0			2.00 352.92
354.25	86213.7		328.6		2	4.00 353.06
354.50	98667.6		373.2		2	8.00 353.19
354.75	111596.0		418.9		2	8.00 353.32
355.00	124524.3		464.7		3	0.00 353.45
355.25	137942.5		511.7		3	2.00 353.59
355.50	151360.8		558.8		3	4.00 353.72
355.75	165355.4		607.7		3	8.00 353.85
356.00	179350.0		656.6		3	8.00 353.99
356.35	200039.7		728.4		4	0.00 354.13
356.70	220729.4		800.1		4	2.00 354.30
356.75	223797.2	64.8	810.7			4.00 354.47
356.80	226865.0		821.3			6.00 354.65
356.90	233083.1	65.9	842.8			8.00 354.84
357.00	239301.2	66.6	864.3			0.00 355.04
	242453.6		875.2			2.00 355.24
357.10	245605.9	67.4	886.1			
357.15	248789.3	67.8	897.1			
357.20	251972.8	68.1	908.0			6.00 355.68
357.35	261714.3	69.2	941.6			8.00 355.91
357.50	271455.7	70.2	975.1			0.00 356.15
357.75	288481.5	72.0	1033.6			2.00 356.39
358.00	305507.4	72.0	1092.1			4.00 356.65
357.25	255220.0	68.5	919.2		6	8.00 358.91
356.50	208906.7	62.8	759.1		6	8.00 357.18
356.75	223797.2	64.8	810.7		7	0.00 357.46
357.00	239301.2	66.6	864.3		7	2.00 357.74
357.00	255220.0	68.5	919.2		7	4.00 358.04
357.20	271455.7	70.2	975.1		7	6.00 358.34
357.50	288481.5	72.0	1033.6		7	8.00 358.65
		73.7				0.00 358.97
358.00	305507.4		1092.1			2.00 359.30
358.25 358.50	419039.7 436919.1	75.4 77.0	1472.2			4.00 359.63
200.00	420212.1	//.0	1533.4			5.00 359.80
					1 0	JU0.500

85.00

359.80

Discharge Rating Curve by Bentley CulvertMaster – Culvert Analysis

*

ANALYSIS JUSTIFICATION - SECTION I-05 (CONT) SERIES OF 30-IN DIA HDPE – DETENTION OUTLET MEETS Q-25 REQUIREMENT

PROJECT: Welsh Run-On & Run-Off Protection Plan\2021 DA Map with H&H Calcs.pro

HYDROLOGIC REPORT

POND OUTFLOW HYDROGRAPH

25 YEAR STORM FREQUENCY TIME RUNOFF (MIN) (CFS) 0.0 0.0 10.0 11.7 20.0 24.8 (MIN) (CFS) MIN MAX IN G = 82.21 cfs	
(MIN) (CFS) 0.0 0.0 10.0 11.7 20.0 24.8	
0.0 0.0 10.0 11.7 20.0 24.8 81	
0.0 0.0 10.0 11.7 20.0 24.8 90 POND INFLOW & OUTFLO 81 A 81 A MAX IN 9 = 82.21 cfs	05)
10.0 11.7 B^{B1} POIND INFLOM & OUTFLOM 20 POIND INFLOM 20 POIND INFL	05)
10.0 11.7	W
20.0 24.8 MAX IN Q = 82.21 cfs	
72 MAX OUT Q = 34.74 cf	
30.0 33.3	5
40.0 34.7	
50.0 33.1	
60.0 30.8 ⁵⁴	
70.0 27.8 80.0 24.9	
80.0 24.9	
90.0 22.0 36 J	
100.0 19.2	
110.0 16.9	
120.0 14.5	
130.0 12.3	
140.0 10.6	
150.0 9.1	
Time (minutes)	261 290
170.0 7.1	
180.0 6.7	
190.0 5.7	
200.0 2.9	
210.0 0.0	
PEAK FLOW = 34.74 CFS	
TIME TO PEAK = 40.00 MIN	
TOTAL VOLUME = 213542.40 CU FT	

ANALYSIS JUSTIFICATION - SECTION I-05 (CONT) I-05 CULVERT: <u>32' X 30" DIA HDPE CULVERT, 8.8' MAX HW DEPTH</u> <u>3.27' CALCULATED HW DEPTH - MEETS Q-25 REQUIREMENT</u>*

TIME	RUNOFF							
(MIN)	(CFS)							
0.0	0.0							
10.0	11.7	Solve For: He	eadwater Elevation		-			
20.0	24.8	Culvert				Inverts		
30.0	33.3		Discharge: 34.74	cfs		Invert Upstream:	343 32	ft
40.0	34.7							
50.0	33.1	Maximum Allov	wable HW: 351.32	ft		Invert Downstream:		ft
60.0	30.8	Tailwater	r Elevation: 0.00	ft		Length:	162.67	ft
70.0	27.8					Slope	0.031229	ft/ft
80.0	24.9	Section				c.opc.		
90.0	22.0	Shape:	Circular	•		- Headwater Elevatio	ns	
100.0	19.2	Material	Corrugated HDPE ((Smooth In 💌		Maximum Allowab	e: 351 32	ft
110.0	16.9							
120.0	14.5	Size:	30 inch	_		Computed Headwate	er: 346.59	ft
130.0	12.3	Number:	1			Inlet Contr	ol: 346.57	ft
140.0	10.6	Mannings:	0.012	-		Outlet Contr	ol: 346.59	ft
150.0	9.1	indianings.	10.0.12					
160.0	7.8	Inlet				Exit Results		
170.0 180.0	7.1 6.7	Entrance:	Beveled ring, 33.7° I	bevels	-	Discharge: 34.74	t i	cfs
190.0	5.7	Ke:			-	Velocity: 15.08	3	ft/s
200.0	2.9	Ne:	0.20			Depth: 1.19		ft

PEAK FLOW =	34.74 CFS	
TIME TO PEAK =	40.00	MIN
TOTAL VOLUME =	213542.40	CU FT

_ _ _ _ _ _ _ _ _

____ _ _ _ _ _ _ _

ANALYSIS JUSTIFICATION CALCULATIONS PERIMETER NON-CONTACT DRAINAGE AREAS

Note: "Perimeter Non-Contact Drainage Areas" refers to storm water runoff from these areas having not come in contact with CCR materials.

ANALYSIS JUSTIFICATION - SECTION P-01 DITCH

0.3% V-DITCH, 3:1 SIDES, 1.8-FT MIN. HW DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE)

HYDROLOGIC REPORT

DEVELOPED UNI Q(PEAK) = C*I		NAL	HYDROG
25 YEAR STORM			
BASIN IDENTIF			
DISCHARGES IN	TO WELSH	ASH	LANDFII
BASIN AREA	= 1.53	AC	CRES
RUNOFF COEFF.	= 0.50)	
RAINFALL INT.	= 8.94	: IN	
TIME OF CONC.) M1	INUTES
	RUNOFF		
(MIN)	(CFS)		
	0.0		
	3.4		
	6.9		
15.0			
20.0	3.0		
25.0	3.0 2.5		
	1.9		
35.0	1.7		
	1.4		
45.0			
	1.1		
	1.0		
60.0	0.9		
65.0	0.9 0.8		
70.0 75.0	0.8		
	0.7		
	0.7		
	0.7		
	0.3		
100.0			
105.0	0.0		
110.0	0.0		
115.0	0.0		
120.0	0.0		
	0.0		
130.0	0.0		
135.0	0.0		
140.0	0.0		
145.0	0.0		0.00
PEAK FLO		5.86	CFS
TIME TO PEA TOTAL VOLUM		.00	
TOTAL VOLUM	E = 10485	.00	CU FT

ANALYSIS JUSTIFICATION - SECTION P-01 DITCH (CONT)

0.3% V-DITCH, 3:1 SIDES, 1.5-FEET MIN. DEPTH AVAIL. MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE) 1.13' CALCULATED HW DEPTH, MEETS Q-25 REQUIREMENT*

Roughness Coefficient	0.030		Flow Area:	3.8	ft²
Channel Slope:	0.003	ft/ft	Wetted Perimeter:	7.2	ft
Normal Depth:	13.6	in	Hydraulic Radius:	6.4	in
eft Side Slope:	3.000	H:V	Top Width:	6.80	ft
Right Side Slope:	3.000	H:V	Critical Depth:	9.6	in
Discharge:	6.90	cfs	Critical Slope:	0.019	ft/ft
			Velocity:	1.79	ft/s
			Velocity Head:	0.05	ft
			Specific Energy:	1.18	ft
			Froude Number:	0.420	
			Flow Type:	Subcritical	

Bentley FlowMaster V8i – Triangular Channel Analysis

*

ANALYSIS JUSTIFICATION - SECTION P-02 0.3% V-DITCH, 3:1 SIDES, 4.0' MIN. DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE)

PROJECT: Welsh Run-On & Run-Off Protection Plan\2021 DA Map with H&H Calcs.pro _____ HYDROLOGIC REPORT _____ DEVELOPED UNIVERSAL RATIONAL HYDROGRAPH Q(PEAK) = C*I*A25 YEAR STORM FREQUENCY BASIN IDENTIFIER P-02 (NDA 01 & NDA 02) DISCHARGES INTO WELSH ASH LANDFILL 4.02 ACRES BASIN AREA = 0.50 RUNOFF COEFF. = RAINFALL INT. = 8.94 IN/HR TIME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) -----0.0 0.0 5.0 9.0 10.0 18.0 P-02 20 г 15.0 13.0 WELSH ASH LANDFILL 20.0 8.0 DEVELOPED 18 25 YEAR STORM 25.0 6.5 MAX Q = 17.97 cfs 16 30.0 5.1 VOLUME = 27460.2 cu ft 35.0 4.4 14 40.0 3.7 45.0 3.3 12 (cfs) 50.0 3.0 10 Runoff 55.0 2.7 60.0 2.5 65.0 2.3 70.0 2.0 6 75.0 2.0 80.0 1.8 85.0 1.8 90.0 1.7 95.0 0.9 15 30 45 60 75 히 105 120 135 150 Time (minutes) 100.0 0.0 105.0 0.0 110.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 0.0 145.0
 PEAK FLOW =
 17.97 CFS

 TIME TO PEAK =
 10.00 MIN
 TOTAL VOLUME = 27460.20 CU FT

ANALYSIS JUSTIFICATION - SECTION P-02 (CONT) <u>1.1%,11.8L/12.6R:1, 10' CHANNEL, AVAIL. 4.0' MIN. HW DEPTH</u> MANNING N VALUE: 0.02 (ROUGHENED CONCRETE) <u>1.63' CALCULATED HW DEPTH</u> -- MEETS Q-25 REQUIREMENT*

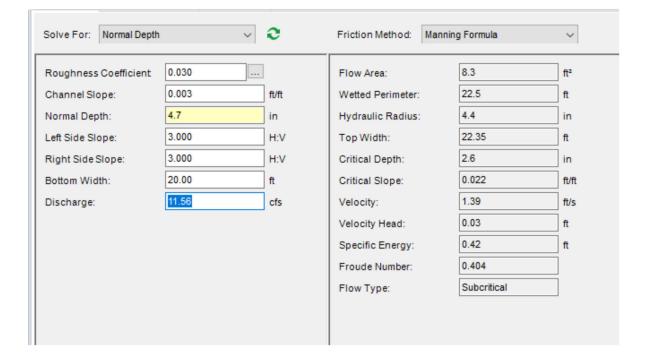
Solve For: Normal Depth	~	0	Friction Method: Mannin	g Formula	~
Roughness Coefficient	0.030		Flow Area:	7.9	ft²
Channel Slope:	0.003	ft/ft	Wetted Perimeter:	10.3	ft
Normal Depth:	19.5	in	Hydraulic Radius:	9.2	in
Left Side Slope:	3.000	H:V	Top Width:	9.74	ft
Right Side Slope:	3.000	H:V	Critical Depth:	14.1	in
Discharge:	18.00	cfs	Critical Slope:	0.017	ft/ft
			Velocity:	2.28	ft/s
			Velocity Head:	0.08	ft
			Specific Energy:	1.70	ft
			Froude Number:	0.446]
			Flow Type:	Subcritical]
1					

* Bentley FlowMaster V8i – Triangular Channel Analysis

ANALYSIS JUSTIFICATION - SECTION P-03 20-FT WIDE, 0.3% CHANNEL, 3:1 SIDES, 7.7-FT MIN. DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE)

HYDROLOGIC REP	PORT		
DEVELOPED UNIV Q(PEAK) = C*I* 25 YEAR STORM	A	AL HYDROGRAPH	
BASIN IDENTIFI			
DISCHARGES INT		SH LANDFILL	
2110 211 111 (211	= 2.59	ACRES	
RUNOFF COEFF.	= 0.50		
RAINFALL INT.		IN/HR	
TIME OF CONC.	= 10.00	MINUTES	
TIME	RUNOFF		
(MIN)	(CFS)		
0.0	0.0		
5.0	5.8		
10.0	11.6		
15.0	8.3		
20.0	5.1		
25.0	4.2		
30.0	3.3		
35.0	2.8	20	P-03 (NDA 03)
40.0	2.4	18 -	WELSH ASH LANDFILL DEVELOPED
45.0	2.2	10	25 YEAR STORM
50.0	1.9	16 -	MAX Q = 11.56 cfs
55.0	1.7		VOLUME = 17658.3 cu ft
60.0	1.6	14 -	
65.0	1.5		
70.0	1.3	12 - 57 A	
75.0	1.3	(s) 9 + 10 -	
80.0	1.2	E	
85.0	1.1	стан	
90.0	1.1		
95.0	0.5	6-	
100.0	0.0		
105.0	0.0	4-	
110.0	0.0	2-	
115.0	0.0		
120.0	0.0	Q	15 30 45 60 75 90 105 120 135 150
125.0	0.0		Time (minutes)
130.0	0.0		
135.0	0.0		
140.0	0.0		
145.0	0.0	EC OTO	
PEAK FLOW			
TIME TO PEAK			
TOTAL VOLUME	<mark>: = 17658</mark> .	30 CU FT	

ANALYSIS JUSTIFICATION - SECTION P-03 (CONT) 20-FT WIDE, 0.3% CHANNEL, 3:1 SIDES, 7.7' MIN. HW DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE) 0.39' CALCULATED HW DEPTH, MEETS Q-25 REQUIREMENT*



* Bentley FlowMaster V8i – Triangular Channel Analysis

ANALYSIS JUSTIFICATION - SECTION P-04 15-FT WIDE, 0.3% CHANNEL, 3:1 SIDES, 6.5-FT MIN. DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE)

DEVELOPED UNIVE 2(PEAK) = C*I*A		AT IIIDKOGI	IVAT U
25 YEAR STORM F	REQUENCY	ערו <u>ג ארו</u>	0 <u>4</u>)
BASIN IDENTIFIE DISCHARGES INTO	WELSH A	ASH LANDFI	LL
BASIN AREA =	6.59	ACRES	
RUNOFF COEFF. =	0.50		
RAINFALL INT. =	8.94	IN/HR	
TIME OF CONC. $=$	10.00	MINUTES	
TIME	RUNOFF		
(MIN)	(CFS)		
0.0			
5.0	14.7		
10.0	29.5		
15.0			
20.0			
25.0	10.7		
30.0	8.3		
35.0	7.2		
40.0	6.1 5.5		
45.0	5.5		
50.0	4.8		
55.0			
60.0			
65.0			
70.0			
75.0			
80.0	3.0		
85.0 90.0	2.9 2.8		
95.0	1.4		
100.0	1.4		
105.0			
110.0			
115.0			
120.0	0.0		
125.0	0.0		
130.0	0.0		
135.0	0.0		
140.0	0.0		
145.0	0.0		
PEAK FLOW	= 29.	46 CFS	
TIME TO PEAK			
TOTAL VOLUME	<mark>= 45016</mark> .	20 CU FT	

ANALYSIS JUSTIFICATION - SECTION P-04 (CONT) 15-FT WIDE, 0.3% CHANNEL, 3:1 SIDES, 6.5-FT MIN. HW DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE) 0.80' CALCULATED HW DEPTH, MEETS Q-25 REQUIREMENT*

Roughness Coefficient	0.030		Flow Area:	13.9	ft²
hannel Slope:	0.003	ft/ft	Wetted Perimeter:	20.0	ft
lormal Depth:	9.6	in	Hydraulic Radius:	8.3	in
eft Side Slope:	3.000	H:V	Top Width:	19.79	ft
Right Side Slope:	3.000	H:V	Critical Depth:	5.7	in
ottom Width:	15.00	ft	Critical Slope:	0.017	ft/ft
)ischarge:	29.46	cfs	Velocity:	2.12	ft/s
			Velocity Head:	0.07	ft
			Specific Energy:	0.87	ft
			Froude Number:	0.447	
			Flow Type:	Subcritical	

* Bentley FlowMaster V8i – Triangular Channel Analysis

ANALYSIS JUSTIFICATION - SECTION P-02 & P-04

P-04 & 02 CULVERTS: <u>28" & 26" DIA HDPE CULVERTS</u> SOLVE AS DETENTION

DROLOGIC REPORT VELOPED UNIVERSAL RATIONAL HYDROGRAPH PEAK) = C*I*A YEAR STORM FREQUENCY SIN IDENTIFIER P-04 6 P-02 COMBINED AT CULVERT - CHANNEL DETENTION SCHARGES INTO WELSH ASH LANDFILL SIN AREA = 10.60 ACRES NOFF COEFF. = 0.50 INFALL INT. = 8.94 IN/HR ME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) 	weish				Map wi	
VELOPED UNIVERSAL RATIONAL HYDROGRAPH PEAK) = C*1*A YEAR STORM FREQUENCY SIN IDENTIFIER P-04 & P-02 COMBINED AT CULVERT - CHANNEL DETENTION SCHARGES INTO WELSH ASH LANDFILL SIN AREA = 10.60 ACRES NOFF COEFF. = 0.50 INFALL INT. = 8.94 IN/HR ME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) 0.0 0.0 5.0 23.7 10.0 47.4 15.0 34.2 20.0 21.0 25.0 17.2 30.0 13.4 35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 115.0 0.0 115.0 0.0 115.0 0.0 115.0 0.0 125.0 0.0 130.0 0.0 131.0 0.0 145.0 0.						
PEAK) = C*I*A YEAR STORM FREQUENCY SIN IDENTIFIER P-04 6 P-02 COMBINED AT CULVERT - CHANNEL DETENTION SCHARGES INTO WELSH ASH LANDFILL SIN AREA = 10.60 ACRES NOFF COEFF = 0.50 INFALL INT. = 8.94 IN/HR ME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) 						
YEAR STORM FREQUENCY SIN IDENTIFIER P-04 & P-02 COMBINED AT CULVERT - CHANNEL DETENTION SCHARGES INTO WELSH ASH LANDFTL SIN AREA = 10.60 ACRES NOFF COEFF. = 0.50 INFALL INT. = 8.94 IN/HR WE OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS)			J HIDROGRAPH			
SCHARGES INTO WELSH ASH LANDFILL SIN AREA = 10.60 ACRES NOFF COEFF. = 0.50 INFALL INT. = 8.94 IN/HR ME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) 						
SCHARGES INTO WELSH ASH LANDFILL SIN AREA = 10.60 ACRES NOFF COEFF. = 0.50 INFALL INT. = 8.94 IN/HR ME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) 	ASIN IDENTIFIE	R P-04 & P-	-02 COMBINED	AT CULVERT -	CHANNEL DE	TENTION
SIN AREA = 10.80 ACRES NOFF COEFF. = 0.50 INFALL INT. = 8.94 IN/HR ME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) 0.0 0.0 5.0 23.7 10.0 47.4 15.0 34.2 20.0 21.0 25.0 17.2 30.0 13.4 35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.2 60.0 6.5 65.0 7.2 60.0 6.5 65.0 7.2 60.0 6.5 65.0 7.2 60.0 6.5 55.0 7.2 60.0 6.5 55.0 7.2 60.0 6.5 55.0 7.2 60.0 4.5 95.0 2.3 100.0 4.5 95.0 2.3 100.0 0.0 115.0 0.0 115.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 145.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	DISCHARGES INTO	WELSH ASE	I LANDFILL			
INFALL INT. = 8.94 IN/HR ME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) 	BASIN AREA =	10.60 /	ACRES			
ME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) 0.0 0.0 5.0 23.7 10.0 47.4 15.0 34.2 20.0 21.0 25.0 17.2 30.0 13.4 35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.8 55.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 115.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 125.0 0.0 133.0 0.0 135.0 0.0 140.0 0.0 140.0 0.0 140.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	RUNOFF COEFF. =	0.50				
TIME RUNOFF (MIN) (CFS) 0.0 0.0 5.0 23.7 10.0 47.4 15.0 34.2 20.0 21.0 25.0 17.2 30.0 13.4 35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 115.0 0.0 120.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 140.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
(MIN) (CFS) $0.0 0.0$ $5.0 23.7$ $10.0 47.4$ $15.0 34.2$ $20.0 21.0$ $25.0 17.2$ $30.0 13.4$ $35.0 11.6$ $40.0 9.9$ $45.0 8.8$ $50.0 7.8$ $55.0 7.2$ $60.0 6.5$ $65.0 6.0$ $70.0 5.4$ $75.0 5.1$ $80.0 4.9$ $85.0 4.7$ $90.0 4.5$ $95.0 2.3$ $100.0 0.0$ $105.0 0.0$ $105.0 0.0$ $115.0 0.0$ $115.0 0.0$ $120.0 0.0$ $125.0 0.0$ $135.0 0.0$ $135.0 0.0$ $140.0 0.0$ $PEAK FLOW = 47.38 CFS$ TIME TO PEAK = 10.00 MIN			4INUTES			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
20.0 21.0 25.0 17.2 30.0 13.4 35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.8 55.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 115.0 0.0 115.0 0.0 115.0 0.0 125.0 0.0 125.0 0.0 135.0 0.0 135.0 0.0 135.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 115.0 0.0 0.0 145.0 0.0 0.0 145.0 0.0 0.0 145.0 0.						
20.0 21.0 25.0 17.2 30.0 13.4 35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 115.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 135.0 0.0 135.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	5.0	23.7				
20.0 21.0 25.0 17.2 30.0 13.4 35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 115.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 135.0 0.0 135.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	10.0	47.4				
20.0 21.0 25.0 17.2 30.0 13.4 35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.8 55.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 115.0 0.0 115.0 0.0 115.0 0.0 125.0 0.0 125.0 0.0 135.0 0.0 135.0 0.0 135.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 115.0 0.0 0.0 145.0 0.0 0.0 145.0 0.0 0.0 145.0 0.0 0.0 145.0 0.0	15.0	34.2				
$25.0 17.2 \\ 30.0 13.4 \\ 35.0 11.6 \\ 40.0 9.9 \\ 45.0 8.8 \\ 50.0 7.8 \\ 55.0 7.2 \\ 60.0 6.5 \\ 65.0 6.0 \\ 70.0 5.4 \\ 75.0 5.1 \\ 80.0 4.9 \\ 85.0 4.7 \\ 90.0 4.5 \\ 95.0 2.3 \\ 100.0 0.0 \\ 105.0 0.0 \\ 115.0 0.0 \\ 115.0 0.0 \\ 125.0 0.0 \\ 125.0 0.0 \\ 135.0 0.0 \\ 135.0 0.0 \\ 145.0 0.0 \\ PEAK FLOW = 47.38 CFS \\ TIME TO PEAK = 10.00 MIN $	20.0	21.0				
35.0 11.6 40.0 9.9 45.0 8.8 50.0 7.8 55.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 135.0 0.0 145.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
40.0 9.9 45.0 8.8 50.0 7.8 55.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 115.0 0.0 115.0 0.0 125.0 0.0 125.0 0.0 125.0 0.0 135.0 0.0 140.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	30.0	13.4				
45.0 8.8 50.0 7.8 55.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0	35.0	11.6				
45.0 8.8 50.0 7.8 55.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0	40.0	9.9				
50.0 7.8 55.0 7.2 60.0 6.5 65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 115.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0 145.0 0.0	45.0	8.8				
65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 115.0 0.0 120.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	50.0	7.8				
65.0 6.0 70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 115.0 0.0 120.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	55.0	7.2				
70.0 5.4 75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 115.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 145.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	60.0	6.5				
75.0 5.1 80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 110.0 0.0 115.0 0.0 122.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
80.0 4.9 85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 110.0 0.0 115.0 0.0 125.0 0.0 135.0 0.0 140.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
85.0 4.7 90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 110.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 140.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
90.0 4.5 95.0 2.3 100.0 0.0 105.0 0.0 110.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 140.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
95.0 2.3 100.0 0.0 105.0 0.0 110.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		4.0				
110.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN		2.3				
110.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN		0.0				
115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN	110 0	0.0				
120.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
130.0 0.0 135.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
135.0 0.0 140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
140.0 0.0 145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
145.0 0.0 PEAK FLOW = 47.38 CFS TIME TO PEAK = 10.00 MIN						
TIME TO PEAK = 10.00 MIN	145.0	0.0				
TOTAL VOLUME = 72408.60 CU FT						
	TOTAL VOLUME	= 72408.60) CU FT			

ANALYSIS JUSTIFICATION - SECTION P-02 & P-04

P-04 & 02 CULVERTS: <u>28" & 26" DIA HDPE CULVERTS</u> 2.42' CALCULATED HW DEPTH AT 28" CULVERT - MEETS Q-25 REQUIREMENT*

PROJECT: Welsh Run-On & Run-Off Protection Plan\2021 DA Map with H&H Calcs.pro _____ HYDROGRAPH RESERVOIR ROUTING POND: P-04 & P-02 COMBINED AT CULVERT T I1 I2 2S1/T 01 2S2/T+02 02 2S2/T _____ 25 YEAR STORM FREQUENCY

 5.00
 0.0
 23.7
 0.0
 0.0
 23.7
 14.3

 10.00
 23.7
 47.4
 9.4
 14.3
 66.2
 31.6

 15.00
 47.4
 34.2
 34.6
 31.6
 84.6
 38.5

 20.00
 34.2
 21.0
 46.1
 38.5
 62.8
 30.3

 25.00
 21.0
 17.2
 32.5
 30.3
 40.3
 21.9

 30.00
 17.2
 13.4
 18.5
 21.9
 27.2
 16.0

 35.00
 13.4
 11.6
 11.1
 16.0
 20.0
 12.5

 9.4 34.6 46.1 32.5 18.5

 17.2
 13.4
 18.5
 21.9
 27.2
 16.0

 13.4
 11.6
 11.1
 16.0
 20.0
 12.5

 11.6
 9.9
 7.5
 12.5
 16.5
 10.4

 9.9
 8.8
 6.1
 10.4
 14.3
 9.2

 8.8
 7.8
 5.2
 9.2
 12.6
 8.2

 7.8
 7.2
 4.5
 8.2
 11.2
 7.3

 7.2
 6.5
 3.9
 7.3
 10.3
 6.7

 6.5
 6.0
 3.6
 6.7
 9.4
 6.1

 6.0
 5.4
 3.2
 6.1
 8.5
 5.6

 5.4
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 5.2

 5.1
 4.9
 2.7
 5.2
 7.5
 5.0

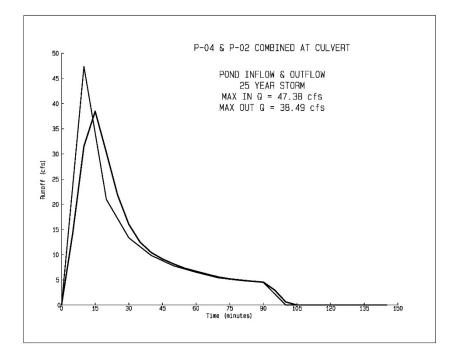
 4.9
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 4.7
 4.5
 2.4
 4.7
 6.9
 4.6

 4.5
 2.3
 2.3
 4.6
 4.5
 3.0

 TIME TO PEAK =
 0.25
 HOURS
 10.25
 10.25

</tabul> 11.1 7.5 6.1 40.00 11.6 5.2 45.00 50.00 4.5 55.00 3.9 60.00 3.6 65.00 3.2 70.00 2.9 75.00 2.7 80.00 2.5 85.00 2.4 90.00 2.3 95.00 1.5 TIME TO PEAK = 0.25 HOURS 38.49 CFS 6920 CU FT MAXIMUM OUTFLOW = MAXIMUM STORAGE = 341.48 FT MAXIMUM ELEVATION = 72409 CU FT INFLOW VOLUME = 72482 CU FT OUTFLOW VOLUME =



ANALYSIS JUSTIFICATION - SECTION P-05 0.3% V-DITCH, 3:1 SIDES & 50'X16" DIA HDPE, MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE) 50'X16" DIA HDPE CULVERT, 8.8' MAX HW DEPTH

		un-Off Protection Plan\2021 DA Map with H&H Calcs.pro
HYDROLOGIC REPOR	RT	
DEVELOPED UNIVER		
Q(PEAK) = C*I*A		
25 YEAR STORM FH	REQUENCY	
BASIN IDENTIFIER		DA 05)
DISCHARGES INTO		
BASIN AREA =		
RUNOFF COEFF. =	0.40	
RAINFALL INT. =	8.94	IN/HR
TIME OF CONC. =	10.00	MINUTES
TIME	RUNOFF	
	(CFS)	
0.0		
5.0		
10.0		
15.0	5.4	
20.0	3.3	
25.0	2.7	
30.0	2.1	
	1.8	
40.0		
45.0		10 r P-05 (NDA 05)
50.0		WELSH ASH LANDFILL
55.0		9- DEVELOPED
60.0 65.0	1.0 0.9	8- MAX Q = 7.49 cfs
70.0	0.9	VOLUME = 11438.1 cu ft
75.0	0.8	7- 1
80.0	0.8	
85.0	0.7	
90.0	0.7	ب بر 5-
95.0	0.4	
100.0	0.0	4-
105.0	0.0	3-
110.0	0.0	
115.0	0.0	
120.0 125.0	0.0 0.0	
130.0	0.0	
135.0	0.0	00 15 30 45 60 75 90 105 120 135 150 Time (ninutes)
140.0	0.0	Lawe Amatorea
145.0	0.0	
PEAK FLOW =		49 CFS
TIME TO PEAK =		
TOTAL VOLUME =	= 11438.3	10 CU FT

ANALYSIS JUSTIFICATION - SECTION P-05 0.3% V-DITCH, 3:1L X 4:1R SIDES, 6.72' MIN. HW DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE) 1.10' CALCULATED HW DEPTH -- MEETS Q-25 REQUIREMENT*

Solve For: Normal Depth	~	e	Friction Method: Mannin	ng Formula	~
Roughness Coefficient	0.030]	Flow Area:	4.2] ft²
Channel Slope:	0.003	ft/ft	Wetted Perimeter:	8.0] ft
Normal Depth:	13.2	in	Hydraulic Radius:	6.3] in
Left Side Slope:	3.000	H:V	Top Width:	7.70] ft
Right Side Slope:	4.000	H:V	Critical Depth:	9.3] in
Discharge:	7.50	cfs	Critical Slope:	0.019	ft/ft
			Velocity:	1.77	ft/s
			Velocity Head:	0.05] ft
			Specific Energy:	1.15	ft
			Froude Number:	0.422]
			Flow Type:	Subcritical]

Bentley FlowMaster V8i – Trapezoidal Channel Analysis

ANALYSIS JUSTIFICATION - SECTION P-05 50'X16" DIA HDPE, 6.72 MIN. HW DEPTH 1.92-FT CALCULATED HW DEPTH – MEETS Q-25 REQUIREMENT

Culvert			Inverts		
D	ischarge: 7.50	cfs	Invert Upstream:	365.12	ft
laximum Allow	able HW: 371.84	ft	Invert Downstream:	363.39	ft
Tailwater I	Elevation: 0.00	ft	Length:	50.00	ft
ection			Slope:	0.034600	ft/ft
Shape:	ìircular	•	- Headwater Elevation	ons	
Material:	Corrugated HDPE (Smooth	In 💌	Maximum Allowab	ole: 371.84	ft
Size: 1	5 inch	-	Computed Headwat	er: 367.04	ft
Number: 1			Inlet Cont	rol: 367.04	ft
Mannings:	.012	•	Outlet Cont	rol: 367.02	ft
let			Exit Results		
Entrance: B	eveled ring, 33.7° bevels	-	Discharge: 7.50		cfs
Ke: 0.	20		Velocity: 10.3	2	ft/s
,			Depth: 0.72		ft

* Bentley CulvertMaster – Culvert Analysis (Used 15" DIA HDPE, Conservative)

ANALYSIS JUSTIFICATION - SECTION P-06 0.3% V-DITCH, 3:1 SIDES & TWO 30-IN DIA HDPE MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE)

PROJECT: Welsh Run-On & Run-Off Protection Plan\2021 DA Map with H&H Calcs.pro _____ HYDROLOGIC REPORT _____ DEVELOPED UNIVERSAL RATIONAL HYDROGRAPH Q(PEAK) = C*I*A25 YEAR STORM FREQUENCY BASIN IDENTIFIER P-06 (NDA 05 & NDA 06 DISCHARGES INTO WELSH ASH LANDFILL 2.50 ACRES BASIN AREA = 0.40 RUNOFF COEFF. = RAINFALL INT. = 8.94 IN/HR TIME OF CONC. = 10.00 MINUTES TIME RUNOFF (MIN) (CFS) -----0.0 0.0 5.0 4.5 10.0 8.9 15.0 6.5 20.0 4.0 P-06 (NDA 05 & NDA 06 10 25.0 3.2 WELSH ASH LANDFILL 30.0 2.5 DEVELOPED 25 YEAR STORM 35.0 2.2 MAX Q = 8.94 cfs 8 40.0 1.9 VOLUME = 13662.0 cu ft 45.0 1.7 7 50.0 1.5 55.0 1.4 6 (cfs) 60.0 1.2 Runaff (5 65.0 1.1 70.0 1.0 75.0 1.0 80.0 0.9 Э 85.0 0.9 90.0 0.8 95.0 0.4 100.0 0.0 105.0 0.0 30 45 120 135 150 60 75 90 105 Time (minutes) 110.0 0.0 115.0 0.0 120.0 0.0 125.0 0.0 130.0 0.0 135.0 0.0 140.0 0.0 0.0 145.0 PEAK FLOW = 8.94 CFS 10.00 MIN TIME TO PEAK = TOTAL VOLUME = 13662.00 CU FT

ANALYSIS JUSTIFICATION - SECTION P-06 (CONT) 0.3% V-DITCH, 3:1 SIDES & MIN 1.92' HW DEPTH MANNING N VALUE: 0.03 (GRASSED – CONSERVATIVE) 1.73-FEET CALCULATED HW DEPTH – MEETS Q-25 REQUIREMENT

Solve For: Normal Depth	~	9	Friction Method: Mannin	g Formula	~
Roughness Coefficient	0.030		Flow Area:	4.5] ft²
Channel Slope:	0.003	ft/ft	Wetted Perimeter:	7.2	ft
Normal Depth:	20.8	in	Hydraulic Radius:	7.5] in
Left Side Slope:	3.000	H:V	Top Width:	5.20] ft
Right Side Slope:	0.000	H:V	Critical Depth:	14.1] in
Discharge:	8.94	cfs	Critical Slope:	0.024	ft/ft
			Velocity:	1.98	ft/s
			Velocity Head:	0.06] ft
			Specific Energy:	1.79] ft
			Froude Number:	0.375]
			Flow Type:	Subcritical]
1					

* Bentley FlowMaster V8i – Triangular Channel Analysis

ANALYSIS JUSTIFICATION - SECTION P-06 (CONT) TWO 84'X30" DIA HDPE, 8.2 MIN. HW DEPTH 0.99' CALCULATED HW DEPTH – MEETS Q-25 REQUIREMENT

Culvert —			Inverts		
	Discharge: 8.90	cfs	Invert Upstream:	356.50	ft
Maximum Allo	wable HW: 364.70	ft	Invert Downstream:	355.20	ft
Tailwate	r Elevation: 0.00	ft	Length:	84.00	ft
Section			Slope:	0.015476	ft/ft
Shape:	Circular	•	Headwater Elevation	ns	
Material:	Corrugated HDPE (Smoo	oth In 💌	Maximum Allowab	le: 364.70	ft
Size:	30 inch	•	Computed Headwate	er: 357.49	ft
Number:	2		Inlet Contr	ol: 357.42	ft
Mannings:	0.012	•	Outlet Contr	ol: 357.49	ft
Inlet			Exit Results		
Entrance:	Beveled ring, 33.7° bevel	s 🔻	Discharge: 8.90		cfs
Ke:	0.20		Velocity: 6.76		ft/s
,			Depth: 0.48		ft

Bentley CulvertMaster – Culvert Analysis

*

Appendix 3: Plan Review Log

Plan Review and Changes in Facility Configuration

Scheduled reviews and Plan amendments shall be recorded in the Plan Review Log below. This log must be completed even if no amendment is made to the Plan as a result of the review.

Ву	Date	Amendment Description	P.E. Certification Required?	P.E. Name	Licensing State Registration No.
RHM	9/13/2021	Complete Reissue *	Yes	Robert H. Murray	Texas 59111

* Significant drainage modifications resulted in major differences require a complete reissue of the Plan

Appendix 4: Professional Engineer Certification

Professional Engineer Certification Page

The undersigned licensed Professional Engineer (P.E.) attests that this Run-on and Run-off Control Plan has been prepared, reviewed, and/or revised in accordance with good engineering practice, including consideration of applicable industry standards and the requirements of 40 CFR 257. This certification in no way relieves the Owner or Operator of the facility of his/her duty to fully implement this Plan.

Engineer:	Robert H. Murray, P.E.	TE OF TOUS
Registration Number:	<u> 59111 </u>	ROBERT H. MURRAY
State:	_ <u>Texas</u>	59111 59111
Date:		CONNAL CAR

P.E. certification is required for the Original Plan and Plan Reviews and Amendments.