# ALTERNATIVE SOURCE DEMONSTRATION REPORT FEDERAL CCR RULE

H.W. Pirkey Power Plant Flue Gas Desulfurization (FGD) Stackout Area Hallsville, Texas

Submitted to



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#### LIST OF ACRONYMS

AEP American Electric Power

ASD Alternative Source Demonstration

CCR Coal Combustion Residuals

CFR Code of Federal Regulations

EBAP East Bottom Ash Pond

EPRI Electric Power Research Institute

FGD Flue Gas Desulfurization

GSC Groundwater Stats Consulting, LLC

GWPS Groundwater Protection Standard

LCL Lower Confidence Limit

MCL Maximum Contaminant Level

QA Quality Assurance

QC Quality Control

SPLP Synthetic Precipitation Leaching Profile

SSL Statistically Significant Level

SU Standard Unit

TCEQ Texas Commission on Environmental Quality

UTL Upper Tolerance Limit

USEPA United States Environmental Protection Agency

WBAP West Bottom Ash Pond

XRD X-Ray Diffraction

#### **SECTION 1**

#### INTRODUCTION AND SUMMARY

This Alternative Source Demonstration (ASD) report has been prepared to address statistically significant levels (SSLs) for beryllium and cobalt in the groundwater monitoring network at the H.W. Pirkey Plant Flue Gas Desulfurization (FGD) Stackout Area, located in Hallsville, Texas, following the first semiannual detection monitoring event of 2020. The FGD Stackout Pad is registered as a waste pile under Texas Commission on Environmental Quality (TCEQ) Industrial and Hazardous Waste Solid Waste Registration No. 33240.

The H.W. Pirkey Plant has four regulated coal combustion residuals (CCR) storage units, including the FGD Stackout Pad Area (Figure 1). In June 2020, a semi-annual assessment monitoring event was conducted at the FGD Stackout Area in accordance with 40 CFR 257.95(d)(1). The monitoring data were submitted to Groundwater Stats Consulting, LLC (GSC) for statistical analysis. Groundwater protection standards (GWPSs) were established for each Appendix IV parameter in accordance with the statistical analysis plan developed for the unit (AEP, 2017) and United States Environmental Protection Agency's (USEPA) Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities – Unified Guidance (Unified Guidance; USEPA, 2009). The GWPS for each parameter was established as the greater of the background concentration and the maximum contaminant level (MCL) or, for constituents without an MCL, the risk-based level specified in 40 CFR 257.95(h)(2). To determine background concentrations, an upper tolerance limit (UTL) was calculated using pooled data from the background wells collected during the background monitoring and assessment monitoring events.

Confidence intervals were re-calculated for Appendix IV parameters at the compliance wells to assess whether these parameters were present at a statistically significant level (SSL) above the GWPSs. Seasonal patterns were observed for beryllium, cobalt, and combined radium at AD-7 and for beryllium, cadmium, cobalt, combined radium, and lithium at AD-22 (Geosyntec, 2020a). To correctly account for seasonality, confidence intervals for these wells and constituents were constructed using deseasonalized values. An SSL was concluded if the lower confidence limit (LCL) of a parameter exceeded the GWPS (i.e., if the entire confidence interval exceeded the GWPS). The following SSLs were identified at the Pirkey FGD Stackout Pad:

- The deseasonalized LCL for beryllium exceeded the GWPS of 0.00400 mg/L at AD-7 (0.00439 mg/L) and AD-22 (0.00635 mg/L); and
- The deseasonalized LCL for cobalt exceeded the GWPS of 0.0560 mg/L at AD-22 (0.0727 mg/L).

No other SSLs were identified (Geosyntec, 2020a).

#### 1.1 CCR Rule Requirements

USEPA regulations regarding assessment monitoring programs for CCR landfills and surface impoundments provide owners and operators with the option to make an alternative source demonstration when an SSL is identified (40 CFR 257.95(g)(3)(ii)). An owner or operator may:

Demonstrate that a source other than the CCR unit caused the contamination, or that the statistically significant increase resulted from error in sampling, analysis, statistical evaluation, or natural variation in groundwater quality. Any such demonstration must be supported by a report that includes the factual or evidentiary basis for any conclusions and must be certified to be accurate by a qualified professional engineer or approval from the Participating State Director or approval from EPA where EPA is the permitting authority. If a successful demonstration is made, the owner or operator must continue monitoring in accordance with the assessment monitoring program pursuant to this section....

Pursuant to 40 CFR 257.95(g)(3)(ii), Geosyntec Consultants, Inc. (Geosyntec) has prepared this Alternative Source Demonstration (ASD) report to document that the SSLs identified for beryllium at AD-7 and AD-22 and cobalt at AD-22 are from a source other than the FGD Stackout Area.

## 1.2 <u>Demonstration of Alternative Sources</u>

An evaluation was completed to assess possible alternative sources to which the identified SSL could be attributed. Alternative sources were identified amongst five types, based on methodology provided by EPRI (2017):

- ASD Type I: Sampling Causes;
- ASD Type II: Laboratory Causes;
- ASD Type III: Statistical Evaluation Causes;
- ASD Type IV: Natural Variation; and
- ASD Type V: Alternative Sources.

A demonstration was conducted to show that the SSLs identified for beryllium and cobalt were based on a Type IV cause and not by a release from the Pirkey FGD Stackout Area.

#### **SECTION 2**

#### ALTERNATIVE SOURCE DEMONSTRATION

The Federal CCR Rule allows the owner or operator 90 days from the determination of an SSL to demonstrate that a source other than the CCR unit caused the SSL. The methodology used to evaluate the SSLs identified for beryllium and cobalt and the proposed alternative source are described below.

## 2.1 **Proposed Alternative Source**

An initial review of site geochemistry, site historical data, and laboratory quality assurance/quality control (QA/QC) data did not identify ASDs due to Type I (sampling), Type II (laboratory), or Type III (statistical evaluation) issues. Groundwater sampling, laboratory analysis, and statistical evaluations were generally completed in accordance with draft TCEQ guidance for groundwater monitoring (TCEQ, 2020). As described below, the SSL has been attributed to natural variation associated with seasonal effects, which is a Type IV (natural variation) issue.

#### 2.1.1 Beryllium

SSLs were identified for beryllium at AD-7 and AD-22 using deseasonalized statistics (Geosyntec, 2020a). According to the Unified Guidance, "seasonal correction should be done both to minimize the chance of mistaking a seasonal effect for evidence of contaminated groundwater, and also to build more powerful background to compliance point tests. Problems can arise, for instance, from measurement variations associated with changing recharge rates during different seasons" (USEPA, 2009).

The seasonal effects observed in the statistical analysis occur in roughly annual cycles, with somewhat higher beryllium concentrations occurring in early spring and lower concentrations in early fall. For example, beryllium concentrations in 2020 at AD-22 were 0.0101 milligrams per liter (mg/L) in March 2020, in contrast to 0.0080 mg/L in June 2020. Previous ASDs for the Stackout Pad showed that beryllium concentrations at AD-22 and AD-7 appear to correlate with groundwater elevations at the wells (Geosyntec, 2019; Geosyntec, 2020b). This relationship still holds true at both AD-22 and AD-7 (**Figure 2**). Beryllium concentrations at AD-7 and AD-22 are both correlated with seasonal changes in other constituents, including calcium (**Figure 3**) and lithium (**Figure 4**). The correlation between beryllium and both monovalent (lithium) and divalent (calcium) cations suggests that the variability in observed beryllium concentrations are related to cation exchange behavior with clay minerals present in the native soil.

Soil borings which were advanced in March 2020 found that clay materials were identified in the seasonally saturated zones above the permanent water table (Geosyntec, 2020b). At AD-7, which was relogged by SP-B2, the depth to water fluctuated between approximately 9 and 15 feet below ground surface (ft bgs). Silty clay was identified from approximately 2.5-6.9 ft bgs before

transitioning to clay until 18.8 ft bgs (**Figure 5**). At AD-22, which was relogged by SP-B4, the depth to water fluctuated between approximately 3 and 12 ft bgs. Clay was identified from approximately 1.5 ft bgs to 13.3 ft bgs, where it transitioned to a clayey silt (**Figure 6**). Analysis by X-ray diffraction (XRD) confirmed the presence of clays within the seasonal water table and sand within the screened interval, as summarized in **Table 1**. The clay fraction of the uppermost samples collected from within the seasonal water table were further analyzed to identify the type of clays present. Smectite-type clays, which are 2:1-layer clays with characteristic cation exchange capacity, make up the majority of the clay minerals present at those intervals.

Sorption and desorption of beryllium from smectite-type clays is well documented (Boschi and Willenbring, 2016a; You, et al., 1989). Desorption was found to be affected by pH, with 75% of beryllium desorbed from a smectite-type clay as pH decreased from 6.0 standard units (SU) to 3.0 SU (Boschi and Willenbring, 2016b). The pH values recorded at AD-7 and AD-22 for samples collected under the Federal CCR Rule ranged from 2.9 to 4.1 SU and 3.9 to 5.1 SU, respectively, suggesting that conditions are favorable for beryllium desorption from smectite-type clays. The presence of these exchangeable clays provides further evidence that the exceedances of beryllium at AD-22 and AD-7 can be attributed to the effects of seasonal groundwater elevation changes, and the resulting cation exchange between groundwater and the exchangeable clay within the seasonal water table, on groundwater quality.

#### **2.1.2** Cobalt

An SSL was identified for cobalt at AD-22 using deseasonalized statistics (Geosyntec, 2020a). As shown in a previous ASD (Geosyntec, 2020b), the cobalt concentrations at AD-22 also appear to correlate with seasonal changes in groundwater elevation (**Figure 7**). The cobalt concentrations are also well correlated with changes in other cations, including calcium and lithium (**Figure 8**), suggesting natural variability associated with interactions with the aquifer solids.

The concentration ratio between calcium and cobalt is consistently on the order of 1000:1 at both upgradient and downgradient locations (**Figure 9**). A sample was collected of the solid FGD sludge material which is accumulated on the Stackout Pad. The solid phase sample was leached using both USEPA's Synthetic Precipitation Leaching Profile (SPLP) testing procedure (SW-846 Test Method 1312) and TCEQ's 7-Day Distilled Water Leachate Test Procedure (30 TAC 335.521 Appendix 4). While cobalt concentrations in both of the leached samples are consistent with those observed in the groundwater samples, the leached calcium concentrations are approximately two to three orders of magnitude higher. However, calcium concentrations in groundwater are generally consistent between AD-22 and upgradient well AD-13 (**Figure 10**). The different ratio between calcium and cobalt in the leached FGD sludge material (about 45,000:1) as compared to the ratio for groundwater indicate that dissolved calcium concentrations at AD-22 would be significantly higher if the groundwater at this location were affected by leachate. The similarity between upgradient and downgradient calcium concentrations, provides an additional line of evidence that the exceedances observed at the FGD Stackout Pad are not due to a release from the unit.

Siderite and pyrite, both reduced iron-bearing minerals, were identified below the seasonal water table (within the saturated zone) at AD-22. Cobalt is known to undergo isomorphic substitution for iron in both siderite and pyrite (Gross, 1965; Hitzman, et al., 2017; Krupka and Serne, 2002). This is due to the similarity of their ionic radii (approximately 1.56 angstrom (Å) for iron vs. 1.52 Å for cobalt [Clementi and Raimondi, 1963). The proposed substitution of cobalt for iron in the crystal lattice of pyrite has been documented in other ASDs prepared for the Pirkey Plant's East Bottom Ash Pond (EBAP; Geosyntec, 2020c) and West Bottom Ash Pond (WBAP; Geosyntec, 2020d).

Goethite (an iron oxide) was identified within the seasonally saturated zone and the screened interval at AD-22 (**Table 1**). The weathering of siderite and pyrite to goethite under oxidizing conditions is a well-understood phenomenon, including in formations in east Texas (Senkayi, et al., 1986; Dixon, et al., 1982) and may have occurred within the seasonally saturated zone. A review of geochemical conditions at AD-22 shows that the conditions observed at AD-22 are favorable for goethite formation (**Figure 11**). During weathering from reduced to oxidized iron minerals, cobalt would be released from the mineral structure. The contribution of cobalt to groundwater via dissolution of siderite or pyrite within the saturated aquifer is not likely to change seasonally. However, the mobilization of cobalt which was released during weathering of siderite or pyrite to goethite in the seasonally saturated zone may explain the variability in aqueous cobalt concentrations and their correlation with the groundwater elevation.

#### 2.1.3 Conceptual Site Model

The seasonal fluctuations in beryllium concentrations at AD-7 and AD-22 and cobalt at AD-22 can be attributed to variations in the amount of the aquifer solids that are in contact with groundwater as the water table elevation changes. When the water table is higher, more clay material is in contact with groundwater, allowing greater desorption of cations (including beryllium) from the cation exchange sites on the clay. In the case of cobalt, more iron oxides are in contact with groundwater as the water table rises, allowing for the release of cobalt from mineral phases where it has isomorphically substituted for iron. Thus, the observed SSLs were attributed to natural variation associated with seasonal desorption of beryllium and cobalt as the amount of aquifer solids that are saturated increases.

#### 2.2 **Sampling Requirements**

As the ASD described above supports the position that the identified SSLs are not due to a release from the Pirkey FGD Stackout Area, the unit will remain in the assessment monitoring program. Groundwater at the unit will continue to be sampled for Appendix IV parameters on a semi-annual basis.

#### **SECTION 3**

#### CONCLUSIONS AND RECOMMENDATIONS

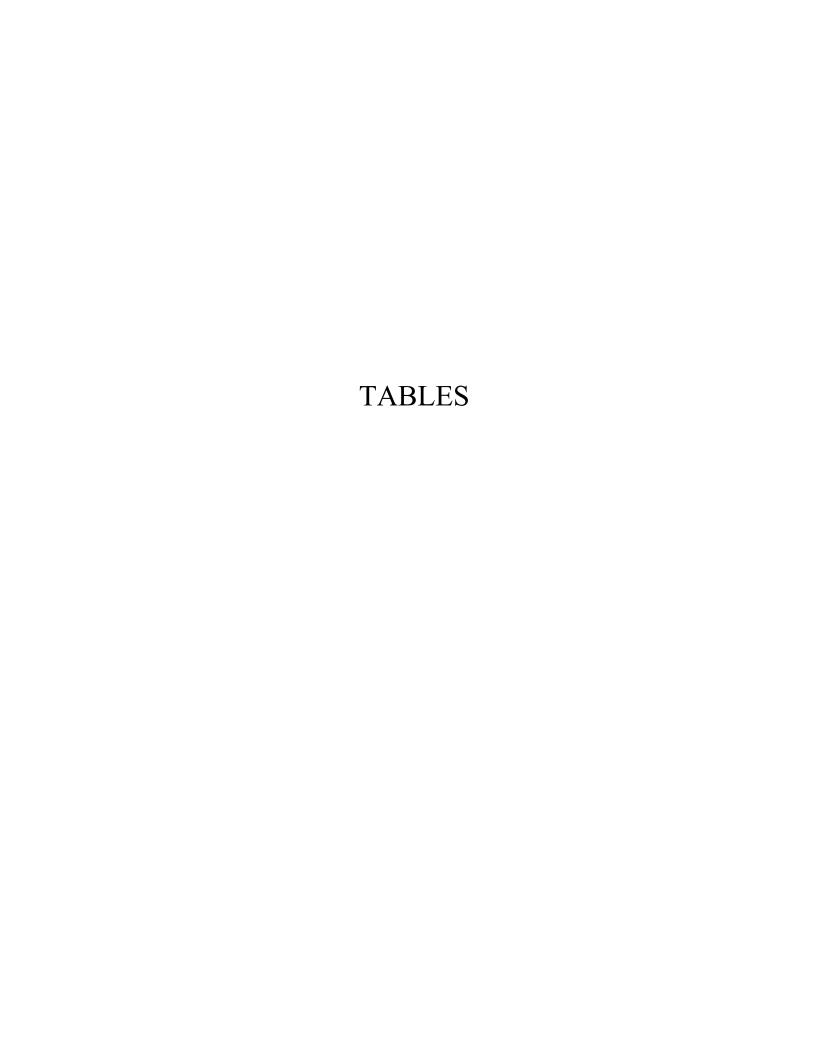
The preceding information serves as the ASD prepared in accordance with 40 CFR 257.95(g)(3)(ii) and supports the position that the SSL of beryllium at AD-7 and cobalt at AD-22 identified during assessment monitoring in June 2020 were not due to a release from the FGD Stackout Area. The identified SSLs were, instead, attributed to natural variation related to seasonal desorption or dissolution of beryllium and cobalt from the aquifer solids. Therefore, no further action is warranted, and the Pirkey FGD Stackout Area will remain in the assessment monitoring program. Certification of this ASD by a qualified professional engineer is provided in **Attachment C.** 

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# Table 1: X-Ray Diffraction Results FGD Stackout Pad - H. W. Pirkey Plant

<b>Boring Location</b>		SP-B2			SP-B4			
Associated Well		AD-7		AD-22				
Depth (ft bgs)	10-12	16-18	27-29	6-8	18-20	28-30		
Sample Location	Within Seasonal Water Table	Below Seasonal Water Table	Within Screened Interval	Within Seasonal Water Table	Below Seasonal Water Table	Within Screened Interval		
Quartz	39	37	79	28	47.5	95		
Plagioclase Feldspar	-	1	-	< 0.5	< 0.5	1		
K-Feldspar	< 0.5	1	-	1	0.5	-		
Goethite	1	2	0.5	1	-	2		
Hematite	-	-	0.5	-	-	-		
Chlorite	-	-	-	1	-	-		
Siderite		-			10	-		
Pyrite	-	-	-	-	2	-		
Clays	*	59	20	*	40	2		
Kaolinite	9			13				
Illite/Mica	1			2				
Smectite	50			43				
Mixed-Layered Illite/Smectite	-			11				

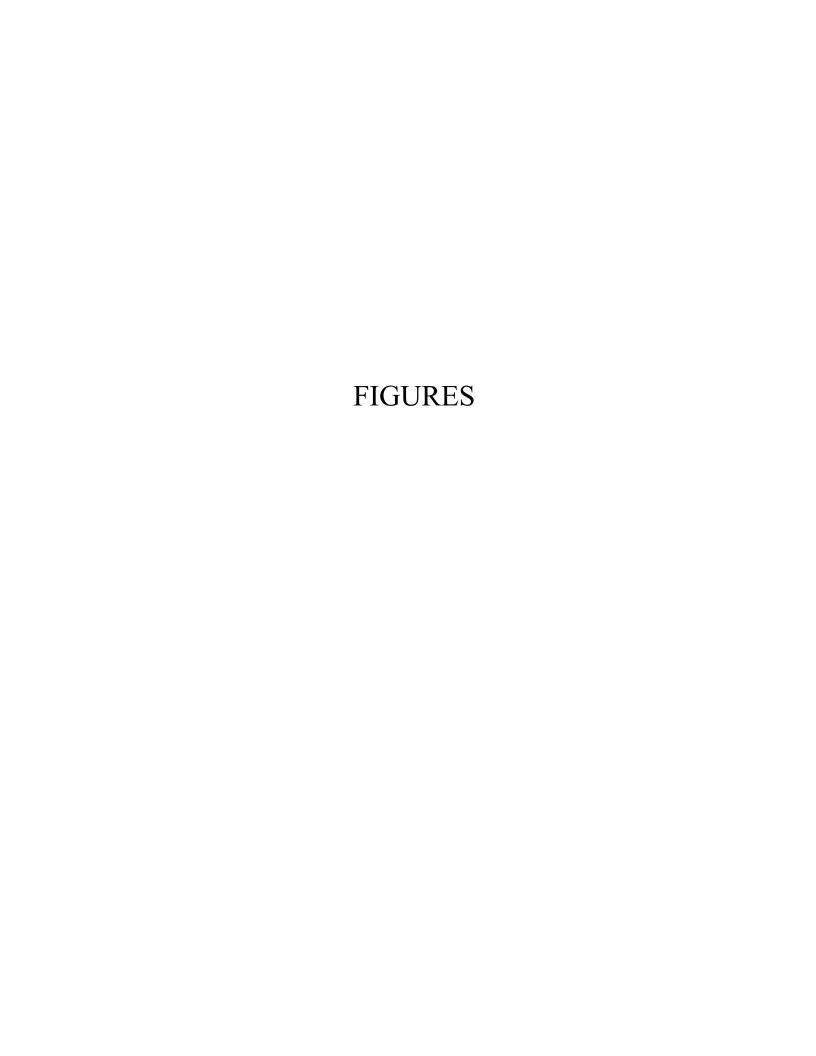
## Notes:

-: not detected

Mineral constituents are reported in percentage.

Values shown as less than indicate the mineral constituent is present but below the quantification limit.

<sup>\*</sup>The clay fraction at SP-B2-10-12 and SP-B4-6-8 were further analyzed to characterize the types of clays present, as listed below.





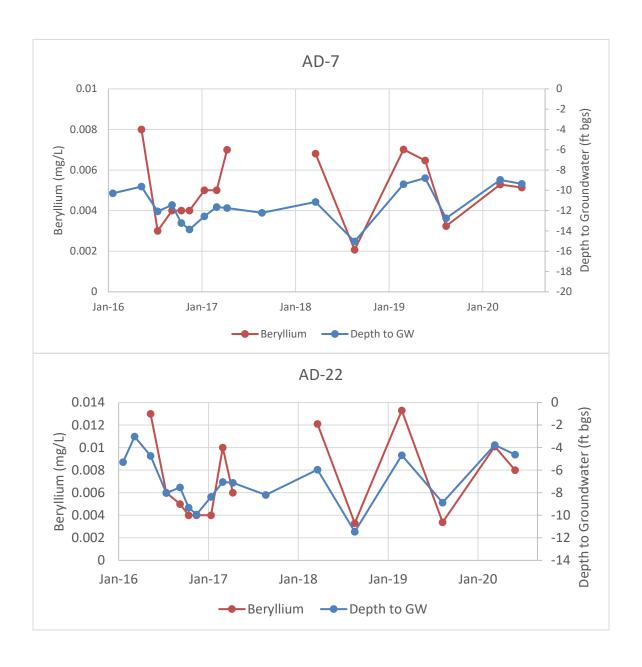
2020 Soil Borings

Stackout Pad

Upgradient Monitoring Well

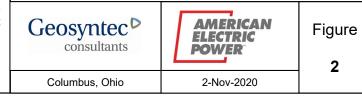
AEP Pirkey Power Plant Hallsville, Texas

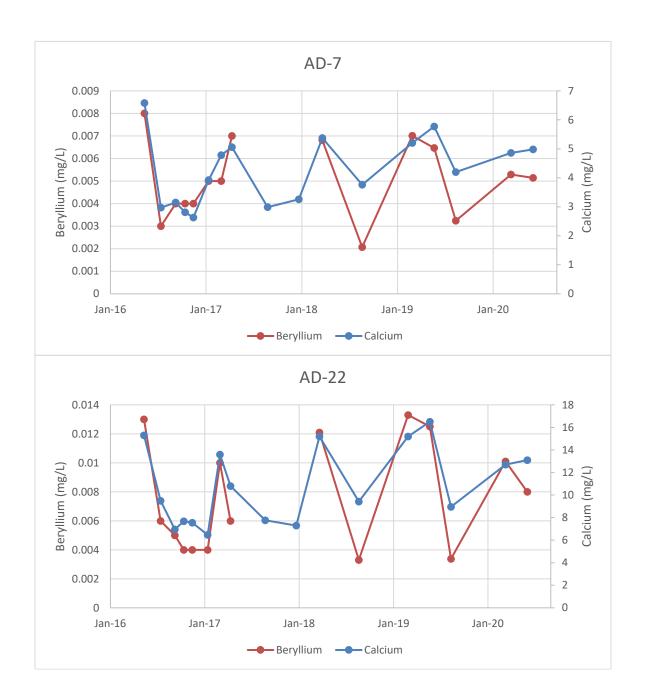
Geosyntec consultants AMERICAN ELECTRIC POWER Figure 1 Columbus, Ohio 2020/03/27



Notes: Beryllium concentrations are shown in milligrams per liter (mg/L). Depth to water is shown as feet below ground surface (ft bgs). The gap in beryllium data represents the time period in which detection monitoring took place and samples were not analyzed for beryllium.

# Beryllium v. Depth to Groundwater Pirkey FGD Stackout Pad



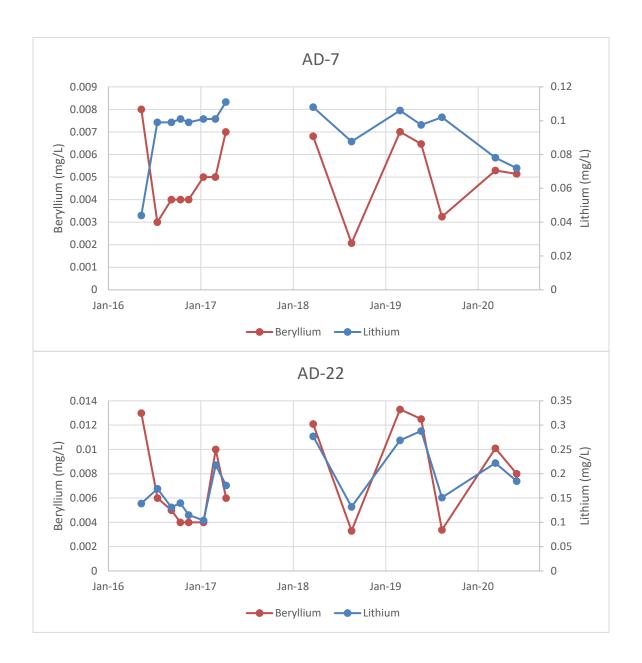


Notes: Beryllium and calcium concentrations are shown in milligrams per liter (mg/L). The gaps in beryllium data represent the time period in which detection monitoring took place and samples were not analyzed for beryllium.

# Beryllium v. Calcium Concentrations Pirkey FGD Stackout Pad

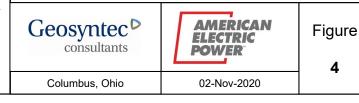
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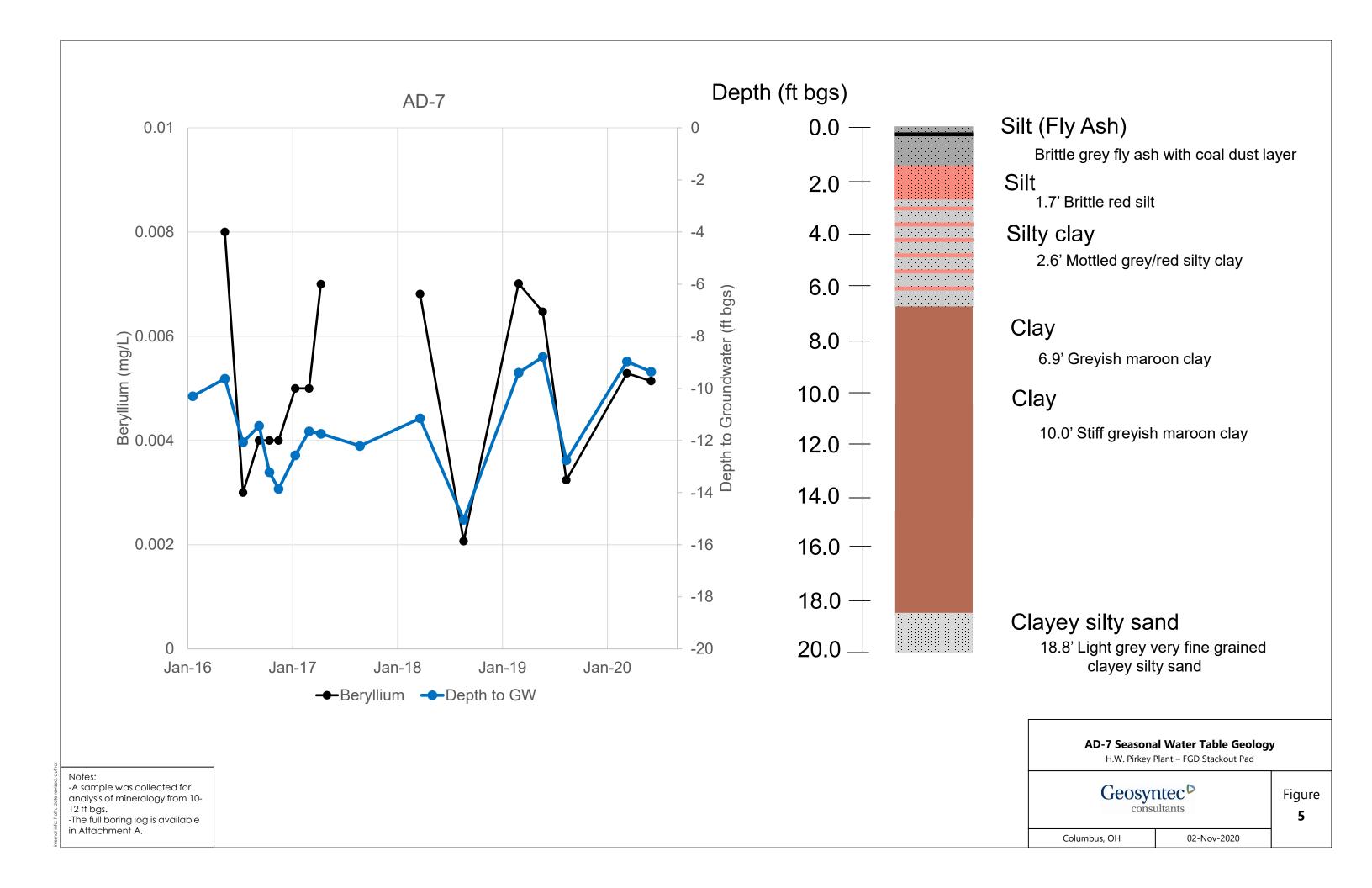


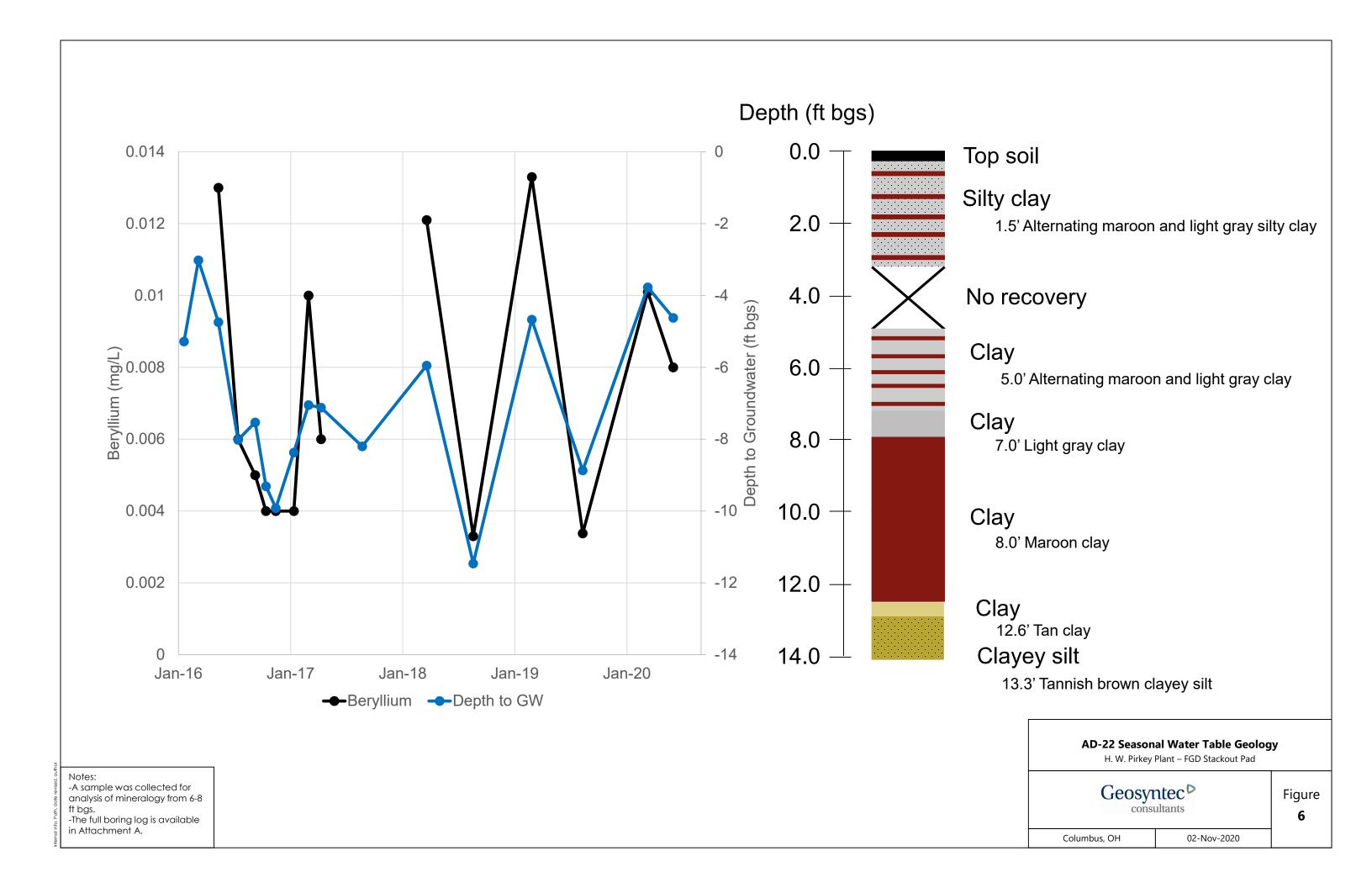


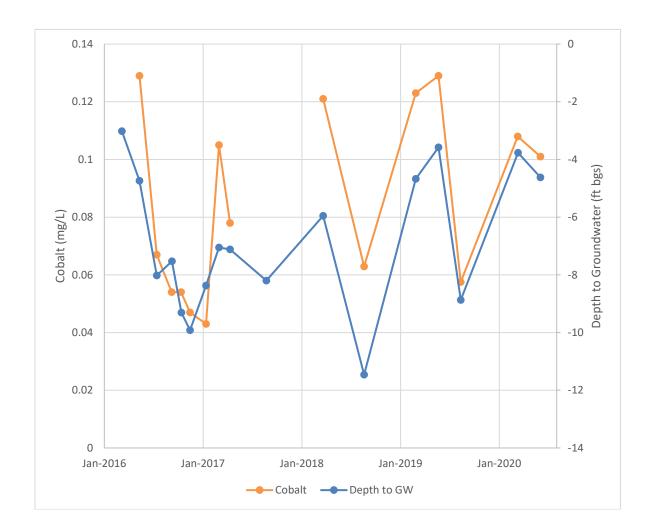
Notes: Beryllium and lithium concentrations are shown in milligrams per liter (mg/L). The gaps in data represents the time period in which detection monitoring took place and samples were not analyzed for beryllium or lithium.

# Beryllium v. Lithium Concentrations Pirkey FGD Stackout Pad



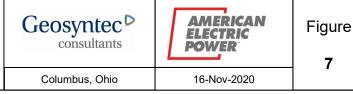


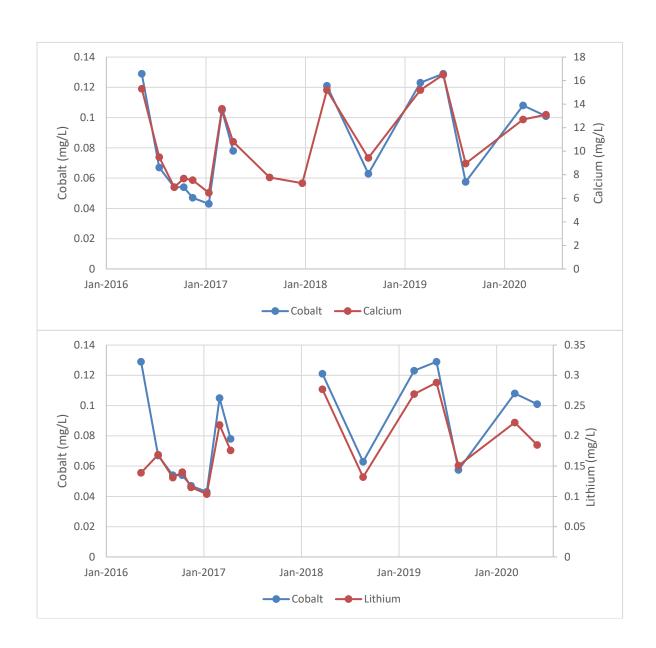




Notes: Cobalt concentrations are shown in milligrams per liter (mg/L). Depth to water is shown as feet below ground surface (ft bgs). The gap in cobalt data represents the time period in which detection monitoring took place and samples were not analyzed for cobalt.

# AD-22 Cobalt v. Depth to Groundwater Pirkey FGD Stackout Pad

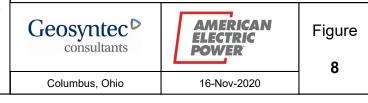


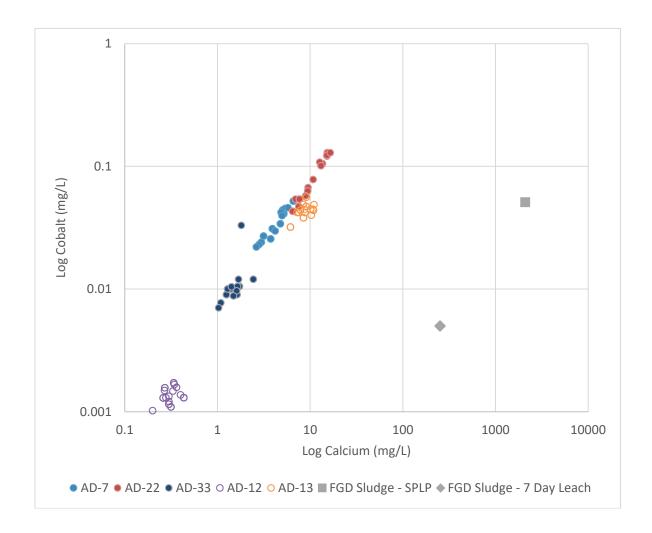


Notes: Cobalt, calcium, and lithium concentrations are shown in milligrams per liter (mg/L). The gaps in cobalt and lithium data represent the time period during which detection monitoring took place and samples were not analyzed for cobalt and lithium.

## AD-22 Cobalt v. Calcium and Lithium

Pirkey FGD Stackout Pad



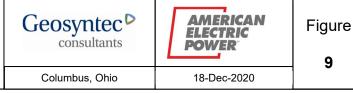


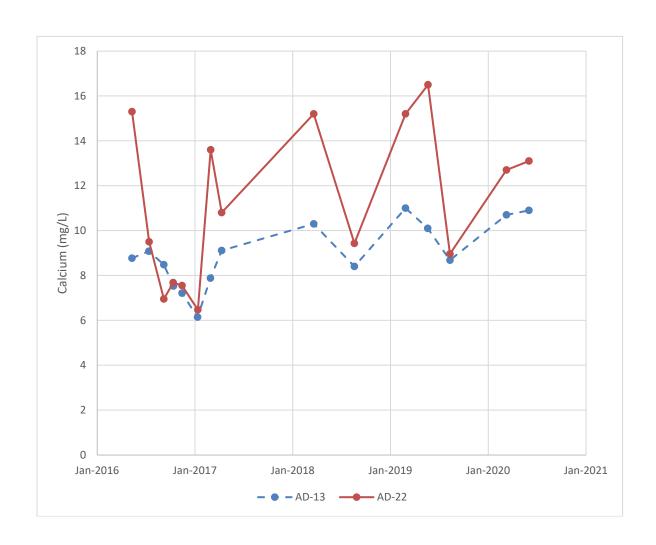
Notes: Cobalt and calcium concentrations are shown in milligrams per liter (mg/L). Upgradient wells are shown with hollow circles. 'FGD Sludge-SPLP' and 'FGD Sludge 7 Day Leach' present the leached concentrations of cobalt and calcium using the Synthetic Precipitation Leaching Procedure (SW-846 Test Method 1312) and the 7-Day Distilled Water Leachate Test Procedure (30 TAC 335.521 Appendix 4), respectively.

## **Cobalt and Calcium Concentration** Distribution

Pirkey FGD Stackout Pad

9

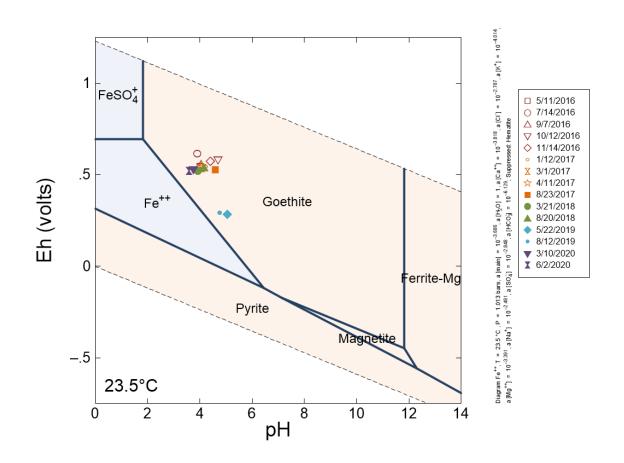




Notes: Calcium concentrations are shown in milligrams per liter (mg/L). AD-13 is shown with a dashed line because it is an upgradient location.

# Calcium Time Series Graph Pirkey FGD Stackout Pad





Notes: Average groundwater concentrations of major cations and anions at AD-22 were used to establish baseline conditions for the diagram. Eh and pH values for sampling dates at AD-22 are shown on the diagram.

# AD-22 Eh-pH Diagram Pirkey FGD Stackout Pad





15-Dec2020

Figure

11

# ATTACHMENT A March 2020 Boring Logs

	Soil Boring Log									
F	Proj	ect	: AEP Pirkey		Boring/Well Name:SP-B1					
F	Project Location:		Location:	Hallsville, TX Boring Date: 3/2/2020						
	Soil Profile		Soil Profile							
oloos Hand	Feet	Water Table		Des	cription	PID*				
	0		pp= pocket pen	etrometer						
	,		0.0'-0.4':	Top soil with vegetation, black silt						
			0.4'-2.1':	Brown silt, fine grained, little cohesion, dry						
ŀ			2.1'-4.3': 4.3'-10.0':		derate stiffness (pp. 3.5); light brown silt/iron ore 4.0-5.0), iron ore (brown/red silt pockets throughout), moist at					
-	5									
<b>-</b> 1	0		10.0'-15.0':	Dark maroon clay, wet, moderate plasticity, m	oderate stiffness (pp. 2.5-3.0), red/brown silt pockets (iron ore)					
- 1	5		15.0'-15.5':	Dark maroon and red/brown clayey silt; low co	phesion; wet					
-			15.5'-20.0':	Light gray and red/brown clayey silt, wet, low	cohesion, iron ore present					
<b>-</b> 2	0		20.0'-21.8':	Dark maroon and red/brown clayey silt; good	cohesion; wet					
l			21.8'-24.0':	Black silty clay, high stiffness (pp. >5.0), low p	lasticity					
Ŀ	5		24.0'-24.5':	Black silty clay, low stiffness (pp. 2.0), modera	ite plasticity					
-			24.5'-30.0':	Dark gray/dark green fine grained sand, well s	corted, trace silt; wet					
- 3	0			Samples collected at 10-12'; 16-18'; 27-29'						
ŀ				TD at 30' bgs *PID readings not collected						
3	5			-						
1	Orilli	ing	Geoprobe 7822 DT Contractor: Ramon Gutierrez		Geosyntec Consultants					

			Soil Bo	oring Log	
Proje	ect:	AEP Pirkey		Boring/Well Name:SP-B2	
⊃roj∈	ect	Location:	Hallsville, TX	Boring Date: 3/2/2020	
		Soil Profile			
Feet	Water Table		Des	cription	*OIA
		pp= pocket pen	etrometer		
,		0.0'-0.2':	Gray silt, dry, brittle (fly ash)		
		0.2'-0.4':	Black, coal dust, strong odor		
		0.4'-1.7':	Gray silt, dry, brittle (fly ash)		
		1.7'-2.6':	red silt, brittle, dry		
		2.6'-6.5':	Gray and red silty clay, high stiffness (pp. 4.0-	5.0), low plasticity, iron ore/mottling present	
		0.51.0.01	Light area, and and top along law stiffness (no	4.5) moderate pleatisity	
		6.5'-6.9':	Light gray, red and tan clay, low stiffness (pp.		
		6.9'-10.0':	Light gray and maroon day, moderate stillnes	s (pp. 3.5), low plasticity, iron ore/mottling present; moist near 9'	
		10.0'-15.0':	Light gray and maroon clay, moderate/high sti	ffness (pp. 3.5-4.5), low plasticity, iron ore/mottling present; wet	
5		15.0'-18.5':	Maroon and light gray clay, moderate/high stif	fness (pp. 3.0-4.0), low plasticity; wet	
		18.5'-18.8':	Red/brown silt, trace clay, good cohesion		
		18.8'-20.5':	Light gray clayey silty sand, very fine grained,	moderate sorting, mottling present; wet	
)		20.5'-23.4':	Light gray and orange clayey silty sand, very f	ine grained; mottling present, moderate sorting; wet	
		23.4'-25.0':	Maroon and orange silty clay, low stiffness (pp	o. 0.5), high plasticity; wet	
5		25.0'-29.0':	Same as above; interchanging between silty of throughout	clay and clayey silt throughout interval, iron ore/mottling present	
		29.0'-29.5':	Black clay, moderate stiffness (pp.3.0), low pla	asticity	
		29.5'-30.0':	Gray fine grained sand, well sorted; wet		
0			Samples collected at 10-12'; 16-18'; 27-29'		
			TD at 30' bgs		
			*PID readings not collected		
5					
	_	Geoprobe 3230 DT		Geosyptes Consultants	
		Contractor: DJ Diduch		Geosyntec Consultants	

	Soil Boring Log								
Proj	ect: AEP Pirke	у	Boring/Well Name: SP-B3						
Proj	ect Location:	Hallsville, TX	Boring Date: 3/2/2020						
	Soil Prof	ile							
Depth Scale Feet	Water Table	De	escription	PID*					
_ ^	pp= pocke	t penetrometer							
- 0	0.0'-0.4':	Top soil, Black silt with vegetation							
_	0.4'-0.7':	Brown silt, moist, low cohesion							
_	0.7'-2.0':	Maroon and light gray silty clay, moderate s	tiffness (pp.2.5), moderate plasticity, iron ore/mottling present						
	2.0'-2.2':	Brown silt, dry, brittle							
	2.2'-5.6':	Maroon and ligh gray clay, high stiffness (pp	o. 4.0), low plasticity						
5.6'-6.0': Orange silt, no cohesion, dry 6.0'-13.5': Maroon clay, high stiffness (pp >4.5), low plasticity; moist at 9'; wet at 12'									
	6.0'-13.5	': Maroon clay, high stiffness (pp >4.5), low pl	asticity; moist at 9'; wet at 12'						
ı 10 ·····									
	13.5'-13.	6': Brown/orange silt (iron ore), no cohesion	sion						
15	13.6'-17.	5': Gray and orange clayey silt, good cohesion;	iron ore present; wet						
	17.5'-20.	2': Maroon and orange silty clay, low stiffness(	pp. 0.5), moderate plasticity; iron ore present; wet						
20	20.2'-21.	1': Brown silt, no cohesion; wet							
	21.1'-22.	7': Brown fine grained sand, well sorted; wet							
	22.7'-25.	0': Maroon and orange silty clay, low stiffness (	pp. 0.5), low plasticity; iron ore present; wet						
25									
30		Samples collected at 10-12'; 15-17'; 22-24'							
		TD at 25' bgs; refusal							
		*PID readings not collected							
35		•							
Drill Drilli	Rig Geoprobe 32 ng Contracto er:_DJ Diduch		Geosyntec Consultants	<u> </u>					

			Soil Bo	oring Log	
Proj∈	ect: AE	P Pirkey		Boring/Well Name:SP-B4	
⊃roj∉	ect Lo	cation:	_ Hallsville, TX	Boring Date: 3/3/2020	
		il Profile			
Depth Scale Feet	Water Table		Des	cription	PID*
	pp:	= pocket pen	etrometer		
0	0.0	0'-0.4':	Top soil, black silt, vegetation		
	0.4	4'-0.7':	Brown clayey silt, good cohesion		
	0.7	7'-1.5':	Red and light gray silty clay, moderate stiffnes	s (pp. 2.5), high plasticity	
	1.5	5'-3.7':	Maroon and light gray clay, high stiffness (pp.	4.5-5.0), low plasticity; iron ore present 3.1'-3.7'	
	3.7	7'-5.0':	NO RECOVERY		
;	5.0	0'-7.0':	Maroon and light gray clay, high stiffness (pp.	4.5-5.0), low plasticity; iron ore present throughout	
		0'-8.0':	Light gray clay with iron ore, moderate stiffnes		
	8.0	0'-10.0':	Maroon clay, moderate stiffness (pp. 3.5), mod	derate plasticity; iron ore present; moist at 9'	
,	10	.0'-12.6':	Maroon clay, moderate stiffness (pp. 3.5), mod	derate plasticity; iron ore present; wet at 12'	
		.6'-13.3':	Tan clay, low stiffness (pp.1.5), high plasticity;		
	13	.3'-18.5':	Tan and brown clayey silt, moderate cohesion	; iron ore present; wet	
	18	5.5'-20.3':	Maroon silty clay, low stiffness (pp. 1.0), mode	erate plasticity; iron ore; wet	
0	20	.3'-21.1':	Dark gray/black clay, trace silt, low stiffness (p	no 1.5) high plasticity wet	<u> </u>
		.1'-21.3':	Dark gray silt, good cohesion; wet	p. 1.0), high plactiony, wor	
		.3'-21.9':	Dark gray silty clay, low stiffness (pp. 1.5), hig	h plasticity: wet	
		.9'-22.3':	Dark gray silt, moderate cohesion; wet	p. actions, net	
		.3'-22.7':	light brown silt; low cohesion; wet		
		.7'-24.4':	_	high stiffness (pp.3.5), moderate plasticity; wet,	
	24	.4'-27.8':	Dark green/gray fine grained sand, well sorted	l; wet; glauconite present	
5	27	.8'-30.0':	Red and orange fine grained sand, well sorted	d, with iron ore; wet	
30					
			Samples collected at 6-8'; 18-20'; 28-30'		
			TD at 30' bgs; refusal		
			*PID readings not collected		
35					
	_	pprobe 3230 DT			
Orilli		ntractor: Diduch	_C&S	Geosyntec Consultants	

Soil Boring Log									
Proj	ect:	AEP Pirkey		Boring/Well Name:SP-B5					
Proj	ect	Location:	Hallsville, TX	Boring Date: 3/5/2020					
0		Soil Profile			T				
Depth Scale Feet	Water Table		Desc	cription	*OIA				
	pp= pocket penetrometer								
0		0.0'-0.6':	Top soil, black silt, vegetation						
		0.6'-0.9':	Brown clayey silt, good cohesion						
		0.9'-2.4':	Red and gray silty clay, moderate/high stiffnes	s (pp. 3.5), high plasticity; iron ore present					
		2.4'-5.0':	NO RECOVERY						
5		5.0'-8.6':	Maroon and gray clay, moderate/high stiffness	s (pp. 3.5), low plasticity; iron ore present; moist					
		8.6'-10.0':	Light gray and maroon clay, moderate/low stiff	fness (pp.2.0), high plasticity; iron ore present; wet					
10		10.0'-12.0':	Maroon and gray clay, high stiffness (pp. 4.0),	moderate plasticity, iron ore present; wet	•				
		12.0'-12.9':	Iron ore with maroon clay, high stiffness (pp.4.	.0), moderate plasticity; wet					
	12.9'-15.0': Maroon clay, high stiffness (pp.4.0), high plasticity; iron ore present; wet								
15		15.0'-18.4':	Light gray and orange clayey silt, good cohesi	on; iron ore present; wet					
		18.4'-18.6':	Dark maroon iron ore; wet						
		18.6'-20.0':	Orange and gray clayey silt, good cohesion; ire	on ore present; wet					
		20.0'-21.2':	Maroon and orange clayey silt, good cohesion	; iron ore present; wet					
.'0		21.2'-22.3':	Black clay, trace silt, low stiffness (pp.1.0), hig	h plasticity; wet	<b></b>				
		22.3'-22.6':	Black clay, high stiffness (pp.4.5), moderate pl	lasticity					
		22.6'-22.9':	Black silt, no cohesion; wet						
		22.9'-23.4':	Black clay, trace silt, moderate stiffness (pp.2.	5), high plasticity; wet					
25		23.4'-25.0':	Dark gray and green fine grained sand; well so	orted; wet; glauconite present					
			Samples collected at 6-8'; 16-18'; 23-25'						
			TD at 25' bgs; refusal						
			*PID readings not collected						
30									
35									
l Drill	Rio	Geoprobe 3230 DT	Г						
Drilli	ing (	Contractor: DJ Diduch		Geosyntec Consultants					

# ATTACHMENT B AD-22 Boring Log and Well Installation Diagram

APEX I	PROJE	CT NO.: _	110-089			□ BORING	BORING NUMBER:		NITOR WELL WELL NUMBER:	AD-22	
FACIL	ITY NA	.ME:	AEP- Pirkey Po	wer Pla	ant			FACILITY ID	NO.: N/A		.
FACIL	ITY AD	DRESS: 1	Hallsville, Texa	ıs					<u>.</u>		.
DRILL	ING CO	OMPANY/	METHOD/RI	G: <u>/</u>	Apex Ge	oscience I	nc. / Hollow-ste	m Augers/ CME-55 Track l	Rig		.
DRILL	ER:	Ed Wilson	ı, Apex Geoscie	nce Inc			COM	IPLETION DATE: 12/10	6/2010		.
PREPA	RED B	Y: David E	Bedford					LOGGED BY: Davi	id Bedford		
LATTI	TUDE:	N 32°27'0	3.3"	I	Datum: \	WGS-84	v	VELL LOCATION: Trian	ngle- South side Quansit Hu	t	
		W94°29'4					•				
DEPTH (FEET)	PID (PPM)	SAMPLE	WELL LO			USCS CODE	5	SOIL DESCRIPTION AND	O COMMENTS	Odor	Moisture
			F	7							
1					0-0.5	SC	Clayey sand, li	ght brown, very fine graine	d	None	Moist
2 3 4 5 6 7 8					0.5-12	CL		t brown mottled with light g		None	Slightly Moist
9 10 11 12 13 14 15 16			V		12-20	SC	very fine grain Slightly wet @	rayish brown with orangish ed ) 12.5' from seepage of iron ore 15-17'	brown streaks,	None	Slightly Wet
17 18 19 20							Very firm 18-	18.5'			
21 22 23 24 25					20-25	SC		line rock 21-21.1'), light br , mica, black clay streaks, v		None	Wet
26 27 28 29 30					25-30	SM	Sand, greenisl very fine grain	a brown (1') grading to oran led	ngish brown, silty,	None	Wet
31 32 33 34 35 36 37 38 39 40							Boring Termi	nated at 30'			
		******	Cement	•		<i>VIIII</i>	_	Filt	ter Sand V Water		,,
geo	⊠Ap oscien	ex ce inc.	Fi		nd (Size it (Type	al Depth: :/Interval) :/Interval) e Comple	: 8-30' : Grout from 0	-2'; Bentonite from 2-8'	Riser Interval: Screen Interval: Water level: Above Ground	+3 (ags)-10 10-30' 12.5' 3'	

# ATTACHMENT C Certification by Qualified Professional Engineer

## CERTIFICATION BY A QUALIFIED PROFESSIONAL ENGINEER

I certify that the selected and above described alternative source demonstration is appropriate for evaluating the groundwater monitoring data for the Pirkey FGD Stackout Area CCR management area and that the requirements of 40 CFR 257.95(g)(3)(ii) have been met.

Beth Ann Gross

Printed Name of Licensed Professional Engineer

Geosyntec Consultants 2039 Centre Pointe Blvd, Suite 103 Tallahassee, Florida 32308

Texas Registered Engineering Firm No. F-1182

79864 Texas

License Number Licensing State 12/31/2020

Date